As-built report for the AH&W Mitigation Site Big and Little Warrior Creeks Wilkes County

Big Warrior Creek before construction, 12/9/98



Little Warrior Creek before construction. 12/11/98





Big Warrior Creek after construction, 1130103



Little Warrior Creek after construction, 1/30/03

North Carolina Wildlife Resources Commission Micky Clemmons and Brent Burgess February, 2003

As-built report for the AH&W Mitigation Site, Big and Little Warrior Creeks, Wilkes County

North Carolina Wildlife Resources Commission

Micky Clemmons and Brent Burgess

February 24, 2003

CONTENTS

Project Objectives

General Construction Narrative

Preconstruction Site Conditions

Channel Modifications

Riparian Improvements

Livestock Management

DATA

Site Map

Livestock Management Practices Installed

Big Warrior Creek Information

Survey

Project modifications

Reference Photo Locations

Photos of Big Warrior Creek

Pebble Count Data

Cross-section & Longitudinal Profile Locations

Cross-section (Dimension) Data

Longitudinal Profile Data

Little Warrior Creek Information

Survey

Project modifications

Reference Photo Locations

Photos of Big Warrior Creek

Pebble Count Data

Cross-section & Longitudinal Profile Locations

Cross-section (Dimension) Data

Longitudinal Profile Data

Water Temperature Data

Locations

Big Warrior Creek

Little Warrior Creek

Project Objectives

The general objectives at this stream mitigation site were to improve water quality, fisheries habitat, riparian quality and stability of Big Warrior and Little Warrior Creeks and the various tributaries to these creeks at this site. A number of activities were undertaken to accomplish these primary objectives. At eroding sections, the stream banks were reshaped to a more stable crosssectional profile. Channels that had been straightened and were incised were modified to a more sinuous pattern with lower banks. Areas of high bank stress were protected using structures or by realigning the channel. Structural improvements were made to improve aquatic habitat. Sections where channel morphology had been destroyed by livestock, had the dimension, pattern and profile reestablished to concentrate flow in a single channel and improve habitat. Disturbed sections of the riparian zone were sloped and planted with native vegetation. Livestock were excluded from the riparian zone to protect vegetation while alternative watering sites and livestock crossings were developed. Initially grasses, sedges, rushes, and other herbaceous vegetation were seeded throughout the riparian zone. During the dormant winter season, bare rooted trees and live stakes of woody species were planted extensively from the bankfull elevation up-slope to the easement line. This project consisted of restoring severely degraded channels as well as the enhancement of channels that were degraded, but morphologically not as badly impacted. Specific objectives for the A, H & W Farm site are described below. The methods used to achieve these objectives are described in the following sections.

- 1. Establish a conservation easement along Big Warrior Creek, Little Warrior Creek and tributaries to allow for the proper dimension, pattern and profile and to protect vegetation and channel morphology.
- 2. Connect Big and Little Warrior Creeks to their floodplains, in areas where they had become incised, by lowering the banks and increasing channel sinuosity (priority 2 restoration).
- 3. Modify dimension and profile along upper Big Warrior Creek to dissipate energy over this steeper reach and realign the channel where it was eroding into steep slopes.
- 4. Increase the pool habitat along both creeks by constructing cross-vane structures.
- 5. Plant native trees, bushes and ground cover that will stabilize the creek banks, shade the stream, and provide wildlife cover and food.
- 6. Enhance fish habitat with structures constructed from natural materials along the primary channels.
- 7. Control existing erosion and sedimentation problems by grading and vegetating problem areas.
- 8. Construct fences and stream crossings where needed to protect the stream riparian buffer established through the conservation easement.
- 9. Install a livestock watering system in fields where cattle are fenced out of the stream, so that the livestock will no longer need to drink from the creek.

General Construction Narrative

Construction at this site was done over a 12-month period with most of Big Warrior Creek being restored under an informal contract with P.G. Park Grading and Little Warrior Creek being restored under a separate informal contract with J & N Mowing. Both of these informal contracts were advertised, a pre-bid meeting was held with potential bidders and the lowest bidder was awarded the contract. Construction on Big Warrior Creek began on August 31, 2001 and ended on November 7, 2001 after 54 days of work. Construction began at the upper easement line and continued downstream to the upper end of the bottom pasture. We stopped work at this point because it was late in the year for vegetation to germinate and grow and the landowner wanted us to stop at a cross fence for the winter. We began construction under the second informal contract on April 22, 2002, and continued until August 30, 2002, for a total of 67 days. We began at the point where we stopped in November and finished Big Warrior Creek in about 2 weeks. At that point we moved to Little Warrior Creek and completed it in the remaining time. Each contractor provided two track-hoes, one rubber tired loader, dump trucks and hand labor, as needed. Access to the site was from Highway 18, Andrews Road SR-1126, farm roads and across the landowner's property. Rootwads were provided by NCDOT from the Highway 441 construction project. We hauled the rootwads to the site under the 1st informal contract and distributed them around the site as needed for construction. Large boulders were purchased from a quarry in Lenoir, NC and hauled to the site as they were needed during construction.

Construction began at the upstream end of each creek and continued downstream with work on the tributaries being done as they were encountered. Vertical eroding banks were sloped, vegetated and erosion control materials installed. Excess soil was moved to sites on the farm where is could be used by the landowner or was used to fill the old channel on Little Warrior Creek. J-hook vanes, cross-vanes, rootwad revetments and floodplain benches were constructed along the channel to improve stability. The upper half of Big Warrior Creek, which had a steeper valley slope, was constructed as a B type channel with cross-vanes creating plunge pools. The lower half of Big Warrior Creek and most of Little Warrior Creek, had a low valley slope and was developed as a C channel with increased sinuosity and an accessible floodplain. Livestock management practices were installed to mitigate the impacts that stream restoration activities would have on the farms activities. These livestock management practices included a watering system that includes a well serving 21 watering tanks across the farm, electric fencing protecting the easement, and stream crossings to move livestock through easement areas. The site was vegetated with a native, riparian seed mix and a cover crop. The cover crop developed well and stabilized the ground surface in spite of the fact that we encountered severe drought conditions during this period. During the dormant period last winter bare rooted trees and live stakes were planted throughout the completed reach on Big Warrior Creek. We have trees ordered for the remainder of Big Warrior Creek and Little Warrior Creek. We also will be harvesting live stakes during March. The trees and live stakes will be planted in March throughout the recently completed areas.

Preconstruction Site Conditions:

Prior to construction the channels at this site were degraded due to past channel dredging, straightening and unrestricted access of livestock. Since construction on each channel was conducted as separate projects, the pre-existing conditions will be described separately.

Big Warrior Creek

Channel Condition - The primary channel is Big Warrior Creek; however, this reach also has three unnamed tributary channels. There was 6540 linear feet of channel on the Big Warrior Creek mainstem, and 2200 linear feet of channel on the 3 tributaries prior to construction. Only one of the tributaries is a perennial stream. Big Warrior Creek at the lower end of the project drains approximately 1.17 square miles, but only 0.7 square miles at the upper end of the site. This appears to make a small difference in cross-sectional area. The one perennial stream that is a tributary drains 0.18 square miles. Pebble count data indicates this stream is dominated by a gravel substrate. A plot of the percentage of the pebble count sample in each size group indicates a bimodal size distribution of bed material (information attached). Most of the sample was composed of course gravel and the smaller component was composed of medium sand. The D_{50} was 11.3 mm and the D_{84} was 50 mm. Although not demonstrated by the pebble data, a fine layer of silt often coated the bottom sediment.

The primary channel transitions from a steep valley (slope=.034, Valley Type II) to a flatter and wider valley (slope=.012, Valley Type VIII) as you move downstream. The stream type that existed here before the channel was degraded is difficult to determine. Based on valley slope, Big Warrior Creek was a B type stream that transitioned to C or E stream type as the valley slope decreased. The channel had been moved over time and had become incised. When the project was being planned the stream type varied over the project reach, and reaches of G, F, B, D and even E could be found at various locations.

Livestock degraded all of these channels. Bankfull was difficult to determine with certainty because livestock had destroyed most indicators. While these streams were adjusting their banks, the smaller tributaries had relatively stable bankfull channels. This is primarily due to the low flows that the tributaries carry and because of the stabilizing influence of vegetation (grasses) on the interberm. The bank height ratios for most cross-sections were high, indicating that the ability of the channel to carry flood flows without damaging the banks is low.

Upper Big Warrior Creek above the bridge had been channelized and moved to the edge of the field. This increased the slope of the channel and caused the channel to become incised at various locations along the reach. The channel had been cut through ridges and was continuing to erode these high clay banks. The upper channel had very little pool habitat and was primarily one long riffle. In the area of the old feedlot, which is just above the bridge, the channel was completely degraded by livestock. Dimension, pattern and profile were completely altered and for most of the reach, the channel was in a braided condition.

Lower Big Warrior Creek below the bridge has a low slope. This reach had been channelized and straightened in the past; however, for the most part it had not become extremely incised. A few stable meanders developed and these were used to evaluate parameters from the reference reach for the design. Most of this section of the creek however, continued to have low sinuosity. The stream was cutting the banks and attempting to reestablish a sinuous pattern. This was moderated somewhat by extensive fescue grass growth on the interberm.

Riparian Condition - The riparian zone was in poor condition. The lower reach of Big Warrior Creek had little or no woody vegetation on its banks. The upper reach had woody vegetation along the north bank but had little herbaceous vegetation under the trees. Lower growing herbaceous vegetation had been damaged or removed by livestock grazing. The south bank was vegetated by pasture grasses only. The tributaries also lack trees and erosion is extensive along

these banks. Cattle had access to all of these creeks and grazing of the riparian vegetation and trampling of the banks had further degraded the riparian area. While the tributaries carry none to low flows for most of the year, they are a major sediment source during periods of high flow. The absence of woody root-mass in the banks results in bank erosion during floods. The lack of woody vegetation also results in the water of these creeks warming beyond a point that will support cold or cool water fish species as demonstrated by the temperature data for August, 2001 and 2002 attached in the data section.

Little Warrior Creek

Channel Condition - The primary channel is Little Warrior Creek; however, this reach also includes three unnamed tributary channels. There was 4610 linear feet of channel on Little Warrior Creek and 3200 linear feet of channel on the 3 unnamed tributaries prior to construction. All three of the tributaries are perennial streams. Little Warrior Creek at the lower end of the project drains approximately .91 square miles, but only 0.43 square miles at the upper end of the site. The lower most unnamed tributary drains from a 5-acre farm pond and contributes approximately the same drainage area (.47 mi²) as LWC at their confluence. Most of this tributaries pre-construction channel was not put in an easement since its alignment was changed and the old degraded channel was filled. Streambed particle data indicates sand and gravel dominate the bedload. A plot of the percentage of the pebble count sample (by count) and subpavement samples (by weight) in each size group indicates a bimodal size distribution of bed material. Two subpavement samples were taken because of the large difference between the 1st subpavement sample and the pebble count. All are plotted in the attached information for comparison. Subsample 2 is considered more representative of the reach. The pebble count is biased toward sand because pebble counts were carried on above normal flow to the bankfull elevation. All particles above base flow stage were sand; however, the base flow channel was more diverse in terms of particle size classes. The heavy vegetation above base flow caused this bias. In our analysis we used the second subpavement sample to represent the bedload, believing that it was more representative of the size of material that moves during a bankfull flow. Most of the sample was composed of small to medium gravel and 30% was composed of sand. The D_{50} was 6.5 mm and the D_{84} was 15 mm.

The project reach is gently sloping with a relatively wide valley (Valley Type VIII) and slope decreases (.013 to .005) and valley width increases as you move downstream. The stream type prior to degradation was difficult to determine. Based on valley slope, Little Warrior Creek was a C or E stream type. The channel had been moved and straightened in the past and had incised. Prior to construction, the stream type varied some over the project reach but was primarily a G type stream. The upper most unnamed tributary was a B or G type channel and primarily carried highway drainage during rain events. It had a number of small headcuts due to the condition it was left in after highway construction and due to the presence of cattle.

Livestock access to all of these streams had degraded the morphology of the channels and eliminated riparian vegetation. Bankfull was difficult to determine with certainty because livestock had destroyed most indicators. While Little Warrior Creek was adjusting its banks, the smaller tributaries were relatively stable. This was primarily due to the low flows that these tributaries carry and because of the stabilizing influence of vegetation (grasses). These tributary channels had also widened and established floodplains. However, the floodplain area is relatively small and steep banks border these small floodplains. The bank height ratios for most cross-sections was high, indicating that the ability of the channel to carry flood flows without damaging

the banks was low. These banks were eroding due to livestock access and needed to be resloped. The upper tributary above the highway culvert, was bordered on the right bank by Highway 18. A steep slope drops from the roadway approximately 30 to 200 feet to the creek. Drainage pipes from this road were causing erosion and litter problems on the slope above the creek and were contributing soil and litter directly to the creek.

Riparian Zone - The riparian zone was in poor condition. The lower reach of Little Warrior Creek (below Andrews Road, SR 1126) had no woody vegetation on its banks. The upper reach had woody vegetation along the south bank but little herbaceous vegetation under the trees. Lower growing herbaceous vegetation had been limited by grazing. Most stream banks were vegetated by pasture grasses to some degree. On Little Warrior Creek, grazing of the riparian vegetation and trampling of the banks was a primary reason for degradation of the riparian area. The tributaries also lacked trees and erosion was extensive along the upper banks were cattle crossed the streams or accessed water. While the tributaries carried low flows for most of the year, they were a major sediment source during periods of higher flows. The absence of a woody root-mass in the banks resulted in bank erosion during floods. The lack of woody vegetation also resulted in the water of these creeks warming to a point that was lethal to cold or cool water fish species native to the stream (information attached).

Channel Modifications:

A reference reach in the immediate vicinity of the AH&W mitigation site could not be located. Design specifications were determined from stable areas on the existing channels, from relic channels in the fields or on floodplains and from a surveyed reference reach on Basin Creek in northwestern Wilkes County (Dan Clinton, personal communication). Reference information was taken from two separate reaches on Basin Creek, a C4 stream that drains areas of 6.8 square miles at one reach and 7.2 square miles at the other. Dimensionless ratios of measurements taken at these sites were compared with information taken onsite. The design was also compared with both the Mountain and Piedmont Regional Curve information. All of this information was used to develop the design for both Big and Little Warrior Creeks. Maps of each channel are attached that show structures installed, pattern modifications made and livestock practices installed during the course of this project. Longitudinal profiles, Cross-sections and photos are also attached that detail the modifications described below.

Big Warrior Creek

Our first approach to restoring upper Big Warrior Creek was to do a priority 1 restoration and reestablish the channel through the field. This would allow for better sinuosity and a floodplain for the channel. However, the landowner would not agree to this, fearing that it would interfere with his existing farming operations. Since the valley slope through this field is rather steep, any new channel would be a B stream type. This stream type could be successfully constructed by modifying the existing channel in place.

A moderately steep reach, such as that found on upper Big Warrior creek above the bridge, will normally not be as sinuous as that found in flatter valleys. Energy that is dissipated through meanders on low slope streams is dissipated by plunge pools on steeper streams. Our approach on upper Big Warrior was to develop a more natural series of riffles and pools. Prior to construction most of this reach was one long riffle with almost no pool habitat. This provided little deep-water habitat for fish and increased erosion of the banks during flooding. Long-term

this can result in an entrenched channel; an example of this existed just above the feedlot. We used boulders, rootwads and logs to create pool habitat along this channel. These materials were used to build structures that provided habitat while at the same time protected the stream banks. In areas with steeper slopes, such as the head-cut halfway up this reach, cross-vane type structures were placed close together to transition through the area. On more gently sloping areas these structures were moved further apart. The attached longitudinal profile shows the increased pool habitat that was created along the channel. In locations where the stream had cut across ridges it had created high, vertical clay banks. We moved the channel away from those banks and developed a floodplain bench at the toe of the vertical slope. The base of this bench was constructed with boulders and this bench was then covered with 1 to 2 feet of soil to allow vegetation to grow. This moved the water off the foot of the clay bank and provided a floodplain bench to dissipate high water velocities and catch any soil that drops from the clay bank. Meanders in the channel were protected using rootwads, and in some cases J-hook vanes. Where the channel was entrenched we lowered the banks and developed floodplains. These modifications can be seen in the attached photos and cross-sections.

The most significant earth moving took place immediately upstream of the upper ford, where the stream was extremely incised. We cut a temporary bypass channel and excavated a new floodplain and channel in the dry. This reach was steep and required a number of cross-vane structures to drop across the slope. Where Big Warrior Creek flowed through the old feedlot, the channel was almost nonexistent. Because of the slope, the B type channel was continued from above through this area, to the bridge. The bankfull elevation on the channel were delineated using coir rolls and soil was filled in behind the rolls. Pools were developed using boulder cross-vanes and log vanes. Overall, our approach on the stream above the bridge was to increase the number of pools, provide access to the floodplain and stabilize the banks by sloping and vegetating them. This should provide habitat and reduce the erosive force of high water.

The flatter reach of Big Warrior Creek (below the bridge) was altered to increase the meandering pattern that it should naturally have. Meanders decrease the slope of the stream, which in turn decrease the erosive force that the stream has during high water events. Meander geometry for this stream was determined by measuring a few stable meanders on the existing channel, by measuring abandoned meanders that are present in the fields and by using measurements from a reference reach. Reference information indicated that for this drainage area belt-width, or width over which the stream meanders, ranged from 45 to 64 feet. This data and landowner concerns lead us to propose an average total easement width of 60 feet. There are areas where existing uses or structures limited the width we could get for a short distance. Other areas allowed for a greater width, but on average, a 60-foot wide easement provided the needed belt-width. The easement along the tributaries has a narrower width since they carry much less flow and in general have a width of approximately 40 feet. The attached surveys show the perpetual easements that are now in place and attached to the deeds of these properties.

Increasing channel meander required that the new channel cross over the existing stream. This required completing the new channel between crossings in the dry, moving as many animals as possible from the old channel to the new one, turning the water from the old channel by blocking the up stream confluence and filling the old channel. Pools were created in the meander bends and riffles constructed to connect pools through the straighter, crossover sections. Areas along the stream bank that receive high stress during flooding flows were protected using rootwads and in some cases rock vanes. Meanders also had coir rolls and blankets installed to provide stability while vegetation developed.

Little Warrior Creek

Our initial approach to restoring Little Warrior Creek was to do a priority-1 restoration and realign the channel through the field. This would allow for greater sinuosity and access to the floodplain by the channel. However, the landowner would not agree to this, fearing that it would interfere with his existing farming operation. The presence of a number of culvert crossings also limited our ability to change the existing channel elevation. A C-type stream was appropriate for this valley type and could be successfully constructed using a priority-2 restoration approach.

On all streams, a primary objective was to reconnect the bankfull channel to its floodplain. This was less of a problem on the tributaries to LWC but was a significant problem on the mainstem. Channelization in the past and down-cutting by the stream had resulted in a very incised condition. Because the stream could not access its floodplain during flood flows, tremendous erosion of the stream banks would occur. Over time, the stream would erode the banks to such an extent that eventually a new floodplain would be established at the elevation of the stream. However, this requires a great deal of time and results in the loss of pasture as tons of soil move down the stream. For this project we lowered the banks along the channel to a bankfull elevation appropriate for the C-type stream that was constructed.

Our approach on the upper unnamed tributary, at the foot of the slope off of Highway 18, was to develop a natural series of riffles and pools. This reach was left by NCDOT as a long straight drainage ditch lined with riprap. This had resulted in a number of small headcuts over the steep section. Long-term this would have resulted in an entrenched channel and excessive sedimentation downstream. We used boulders to create cross-vanes and plunge pools along this steep reach were the headcuts were found. This should result in energy dissipation during storm flows and provide wetland habitat during other times. The boulder structures should arrest any further head cutting.

The other tributaries and the mainstem of Little Warrior Creek are flatter and were altered to increase the meandering pattern that should naturally be found. Meander geometry for these streams was similar to that used for Big Warrior Creek and varied slightly as drainage area changed. The smaller channel above the confluence with the pond tributary has a meander length of 135-feet and an average radius of curvature of 25-feet. LWC below the confluence has approximately twice the drainage area and had a meander length of 200-feet with an average radius of curvature of 50-feet.

Construction of meanders that moved back and forth across the existing channel followed the same approach as was used on Big Warrior Creek, with construction being completed from meander to meander before the next section was started. In locations where the stream cut across ridges, it had created high, vertical clay banks. There were a couple of these sites on LWC above Andrews Road, S.R. 1126. We moved the channel away from the banks and built a floodplain bench at the foot of the bank. The bench was constructed of small boulders placed at or below the bankfull elevation. The boulders were then covered with soil and compacted to form a surface that was vegetated and matted with erosion control materials.

The first tributary to Little Warrior Creek drains out of a farm pond, flows under S.R. 1126 and, prior to construction, then flowed down the pasture for 400 feet to the confluence. Over that distance the two channels ran parallel approximately 100 feet apart before coming together. Both channels had been straightened in the past and were incised, with low habitat value. We moved the pond tributary channel so that it connected to Little Warrior Creek higher in the pasture and just below Andrews Road. The new channel is a meandering channel or S curve with

a low slope through the meanders and then drops over a series of rock cross-vanes. It has a total length of approximately 170 feet. The old channel was filled with soil excavated from stream banks on the project. This resulted in a loss of 400 feet of degraded, incised channel and the gain of 170 feet of naturally designed channel that will have good to excellent habitat value over time. This channel change was done as the last channel work on the project so that access could be maintained into the field. To facilitate access so that channel work could be done and the old channel filled the stream was placed in a temporary bypass channel until the new floodplain and channel could be constructed. This temporary channel was lined with synthetic erosion control cloth and had a number of check dams constructed through its length. This was all removed as the final channel change was done to connect the tributary to Little Warrior Creek.

The greatest obstacle to restoring the channel on Little Warrior Creek was the soils that we encountered at this site. There was very little rock in them and they tended to wash easily. There was also a great deal of clay present. This caused problems in two ways: vegetation grows poorly in these soils and the soil tends to wash out from around the structures. We did get a good stand of the cover crop in the fields and on the side slopes, but not as good on the constructed floodplains. We are continuing to work with these areas and believe that the perennial mix will do well as it develops. The day construction was completed we had a 2 to 3 inch rain in about 1 hour. This caused problems around the structures that stepped down the cross over channel to Little Warrior Creek and to the structure we constructed to raise the pool and eliminate the drop below DOT's culvert under Andrews Road. It appeared that the soil dissolved away as the bed below the structures completely mobilized during the high water event. We repaired these structures by placing filter fabric in front of the structures and filling in front of the structures with a layer of riprap size rock, then a layer of large washed stone. This was then buried with the bed material. There have been a number of high water events since these repairs were made and the structures seems to be in good shape.

Riparian Improvements:

Riparian improvements were common to both Big Warrior Creek and Little Warrior Creek and included the following practices. The stream was reconnected to the floodplain, which resulted in a natural condition where high water will overflow the floodplain reducing water velocity, causing suspended soil to deposit, enriching the soil and improving water quality. Banks at the back of the created floodplains were graded to approximately a 2:1 slope. At the interface between the bankfull channel and the floodplain, biodegradable erosion control materials were used to provide stability while vegetation grew. After the creek bank had been shaped and before erosion control materials were installed, it was limed, fertilized and seeded. A temporary ground cover of millet, wheat, or barley was seeded under the erosion control blankets. Due to extremely dry conditions these areas were then watered using a gas powered water pump so that quick germination would occur. A perennial seed mixture was also planted under these erosion control materials (Table 1). We expect this mixture to be slow in developing and recognize that it is often 1 to 2 years before a good stand of the perennial plants develop. This mixture was planted throughout the easement area. In addition to the seed mixtures, during the dormant season of late winter, the riparian area close to the creek was planted with native woody species such as alder, willow, dogwood and button bush. On the upper banks, we planted taller growing trees that will provide shade, wildlife cover and food, and stability to the creek banks. Woody species were planted as bare-rooted trees and live stakes. Plantings on Big Warrior Creek took place in winter 2002 and Little Warrior Creek will be planted in winter 2003.

Areas of the channel that were incised had the floodplain reconnected to the stream by excavating the existing banks within the easement down to the bankfull elevation. Banks were protected by structural modifications when needed and by erosion control materials such as coir rolls and coir matting. Coir rolls were used to establish a bankfull elevation where this had been degraded and around the outside of meanders. Coir and Jute matting was used as ground stabilization along the entire new channel. Straw was used in seeded, bare ground areas outside of the channel. The easement along the upper tributary of Little Warrior Creek includes a wide sloping area from Highway 18 down to the stream. The soil of this slope is unproductive red clay, fill material. It has been grazed since originally constructed, so little vegetation has developed. In addition water running off of the highway had caused erosion problems in a number of areas due to drainage pipes that extended only partway down the slope. These drainage culverts were extended to carry runoff down the slope to the channel. Screened settling basins at the mouths of the drainage culverts, were located along the banks of the stream to capture litter washing from the roadway. Some trees were planted along this slope during the winter of 2002 and additional trees will be planted in 2003. This area will be managed for slope stability, safety on the roadway and maximum wildlife benefits from the vegetation.

Table 1. Native Riparian Seed mix sewn throughout the easement area at the AH&W mitigation site.

Sitt.	
Plant	Botanical Name
Sunburst Switchgrass	Panicum virgatum
Partridge Pea	Chamaecrista fasciculate
Slender Smartweed	Polygonum lapathifolium
Lance-leaved Coreopsis	Coreopsis lanceolata
Smartweed	Polygonum pennsylvanicum
Smooth Panicgrass	Panicum dichotomiflorum
Virginia Wild Rye	Elymus virginicus
Osage Indiangrass	Sorghastrum nutans
Southern Arrowwood	Viburnum dentatum
Biannual Evening Primrose	Oenothera biennis
Bur-Marigold/Showy Tickseed	Bidens aristosa
Little Bluestem	Andropogon scoparius
Big Bluestem	Andropogon gerardii
Silky Dogwood	Cornus amomum
Ashy Sunflower	Helianthus mollis
Buttonbush	Cephalanthus occidentalis
River Oats	Uniola latifolia

Livestock Management:

An important part of this stream mitigation plan is the exclusion of livestock from the riparian zones of Big and Little Warrior Creeks and their tributaries. In large part, livestock management will determine the success of the total project. The Natural Resource Conservation Service (NRCS) developed a livestock management proposal in consultation with the Farm management and the North Carolina Wildlife Resources Commission (NCWRC). These plans are for the entire farm and include addressing issues on all watercourses on the farm. The estimated total cost of the livestock practices proposed for this site is \$115,689.00. These are broken down among the

landowners as follows: Andrews - \$67,101, Weston - \$37,838, all others - \$10,750. The attached map of agricultural practices details the practices that have been and are being installed. The landowner or a designated contractor hired by NRCS can do the installation of these practices. At this site the landowners chose to do the installation. The have completed many of the planned activities but still have some fencing to complete and a few watering tanks to install. The NRCS administers construction of all phases of this part of the mitigation plan. The WRC and NRCS will monitor the functioning of these practices during their initial 2 years of operation. After this period, the landowner is responsible for those practices that are not within the easement. This primarily refers to the watering system. The NCWRC will continue to maintain the fence and crossings. Landowners are expected to do minor fence and crossing maintenance, which may be required, such as tightening due to cattle pushing the wire, farm equipment damaging the fence or gates and removing debris that may block crossings.

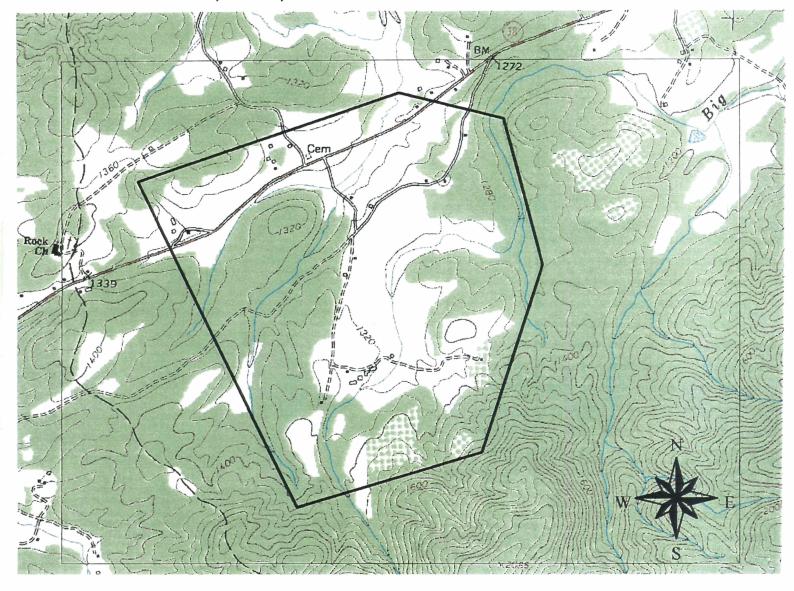
Fencing: Approximately 28,000 linear feet of fencing has been or is being installed to protect the easement at this site. The map of the site, shows the location of fencing. We are fencing livestock out of all streams within the easement. This will include any length of the easement line along each primary stream and their tributaries where livestock might access the easement area. In those areas where cattle will not be pastured a fence is not required, for example on upper Big Warrior Creek were the cattle will only be on the pasture side of the easement or on upper Little Warrior Creek were the cattle will be on the pasture side of the easement and not in the woods. Where no fence is constructed, a provision in the easement agreement leaves this option open to the NCWRC if it is needed to protect the easement in the future. Five tributaries have crossings proposed and to install the crossings we will have to protect the channels with an easement and fencing. The proposed fence is a permanent, high tensile electric fence.

Watering facilities: The fencing needed to protect the easement will remove the water source livestock presently use on this farm. A watering system has been installed that should provide sufficient water for the number of cattle that these pastures can support. This should provide better quality drinking water than the creeks and improve livestock health. Twenty-one watering tanks are being installed on the entire farm. The division of these tanks by pasture can be seen on the accompanying map. A well was drilled and connected to existing farm wells to supply water under pressure to all of the watering tanks on the system. Tanks are rectangular two or four hole tanks, constructed of thick walled plastic. The tanks are insulated and should not freeze if the cattle use them enough to keep water flowing through the system. Water supply lines are all buried and should not freeze. Tank locations are hardened for high use and kept well away from the easements.

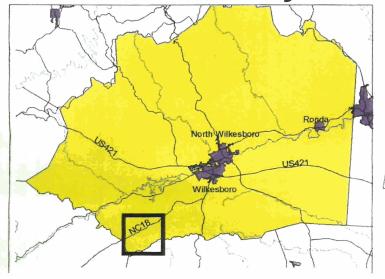
Cattle Crossings: To facilitate cattle moving from pasture to pasture through the easement, a number of stream crossings were installed. Three culvert crossings were installed on the small tributaries to Big Warrior Creek. These were sized to be sufficient for carrying the 10-year storm. Culvert crossings installed at this mitigation site consisted of a large pipe that carries base flow as well as storm flow and a smaller culvert placed at the bankfull elevation to carry storm flow that is moving across the floodplain. Two existing culverts in the upper pasture on Big Warrior Creek w be extended so cattle can pass over these tributaries. These crossings are to be managed by being open, as farm operations dictate. The bridge below the present feedlot was upgraded with decking so that it can be used to move cattle from one side of Big Warrior Creek to the other. Future maintenance of this upgraded bridge is the responsibility of the landowner. Two ford type crossings were installed on Big Warrior Creek at the lower end of the upper pasture and in the middle of the lower pasture. These fords were constructed using a 4-inch Terracell structure that

was back-filled with stone. Below each structure a cross-vane was built to maintain the grade across the crossing. The fords should be maintained as limited access crossings and opened to move cattle from pasture to pasture, but not left open for cattle to use at will. The reason for this is that one objective of this project is to improve water quality and if cattle have constant access to the stream there will be water quality degradation. A culvert crossing was installed on the small tributary to Little Warrior Creek below the Ham house. This culvert was built in the same way as the Big Warrior culverts were constructed. Four ford type crossings were installed on LWC. One ford was built at either end of the large box culvert under Highway 18 and two at the top on each end of a cattle trail built around a narrow section on upper Little Warrior Creek near Highway 18. These last two crossings will allow the cattle to move along a cattle trail through the woods and up to the upper pasture on LWC, while keeping them out of the easement. These will be stoned crossings, gated to limit access. Two existing culverts under Highway 18, in the upper pasture on Little Warrior Creek, were extended so cattle can pass over these tributaries, while allowing the rest of the tributary to be fenced.

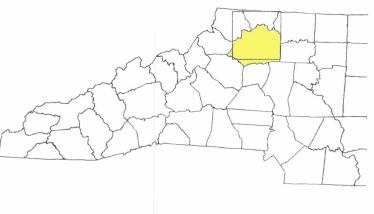
A, H, & W Farm Site



Wilkes County



North Carolina

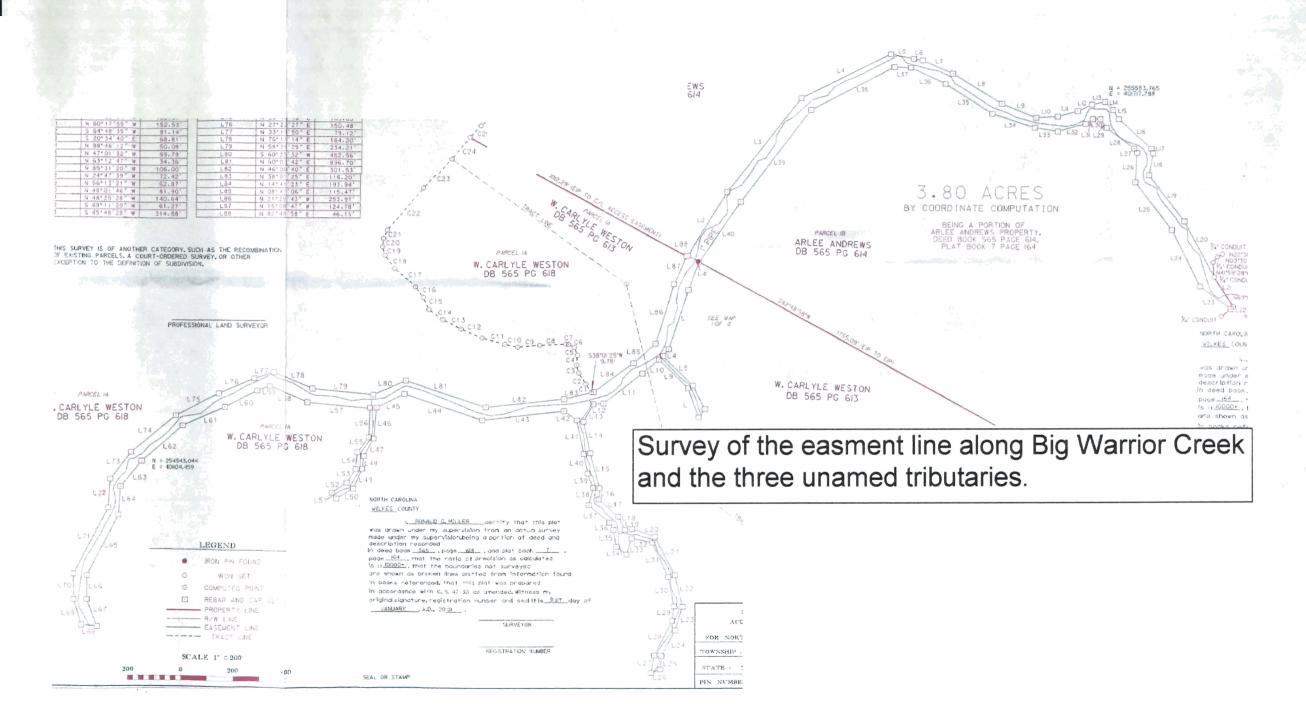


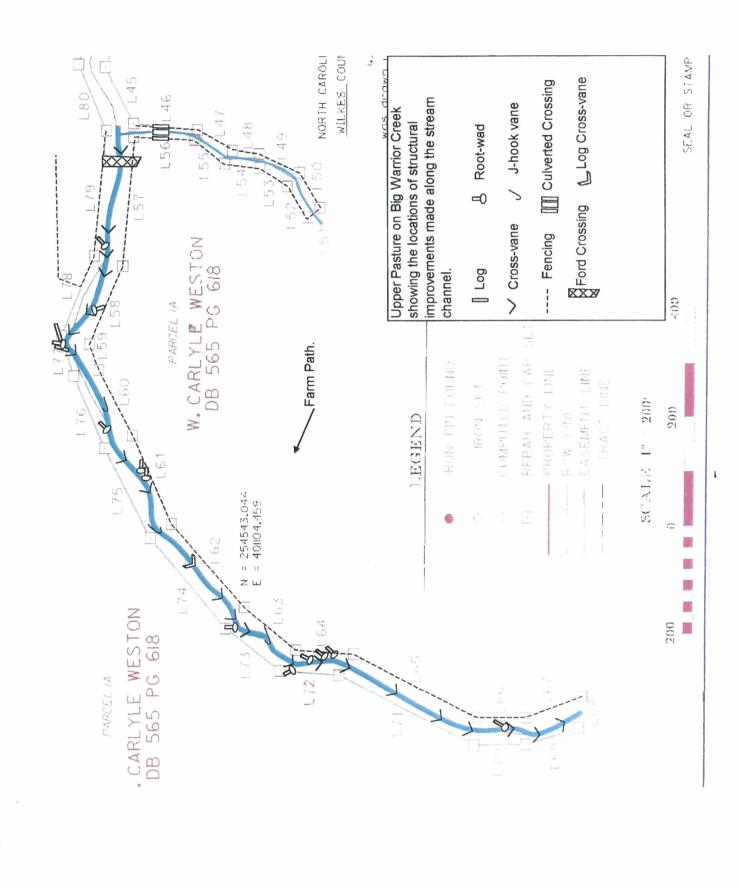


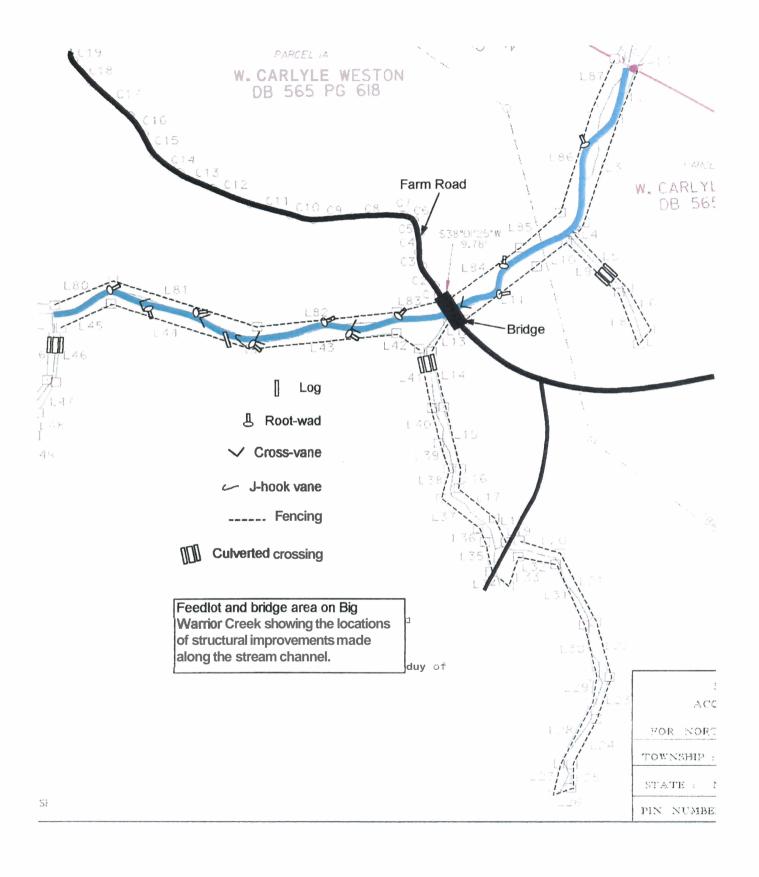
Livestock Management Practices Installed at the AH&W Mitigation Site

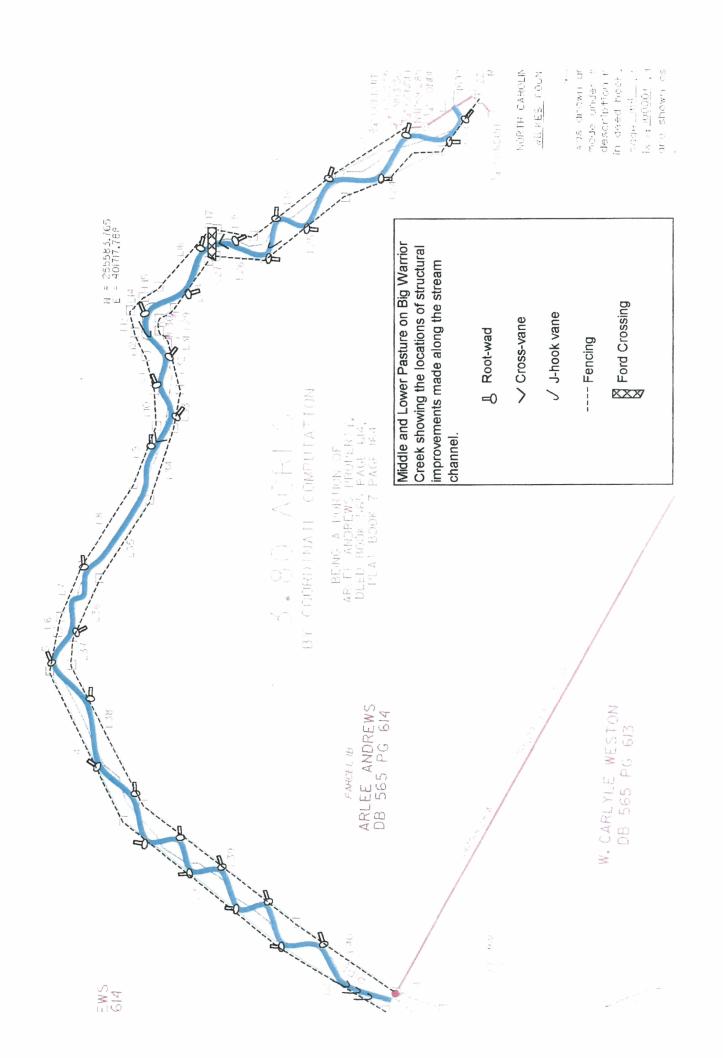
Big Warrior Creek As-built Stream Restoration Data

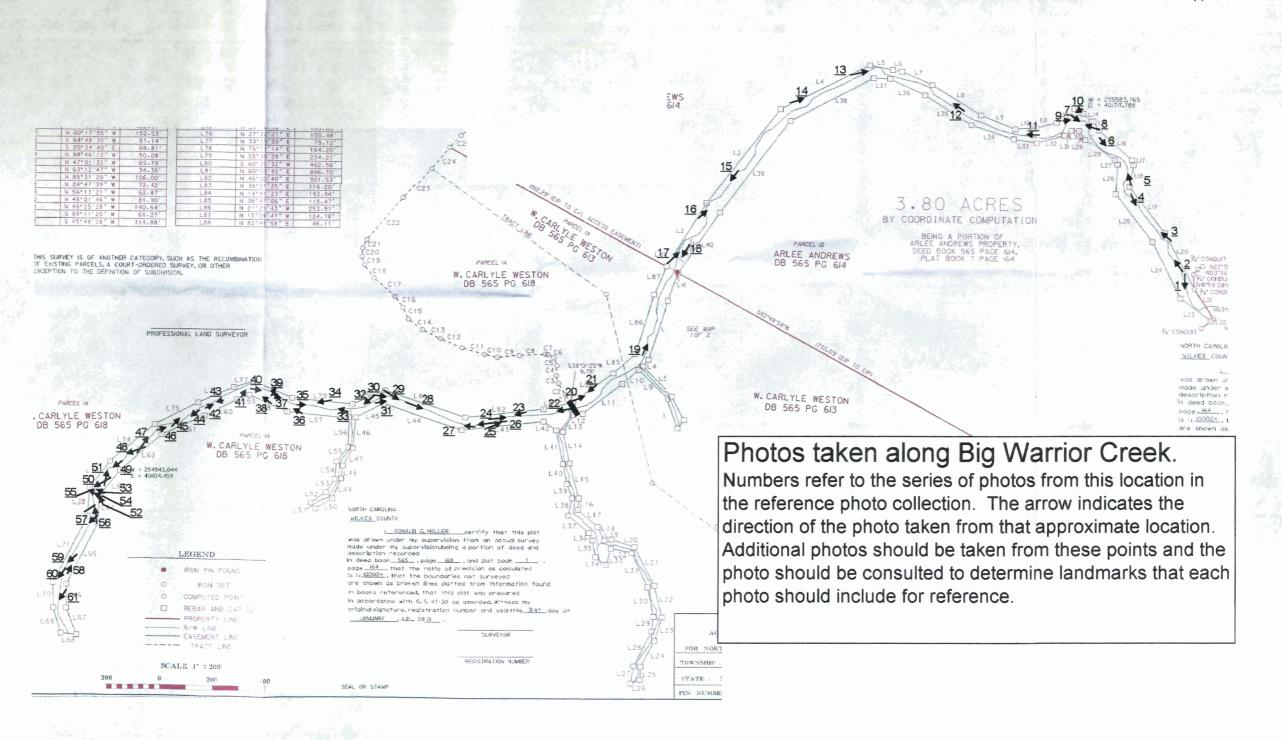
Survey
Project modifications
Reference Photo Locations
Photos of Big Warrior Creek
Pebble Count Data
Cross-section & Longitudinal Profile Locations
Cross-section (Dimension) Data
Longitudinal Profile Data













Mvc-003s, AH&W 98-12-9



DSC00243, 3/1/30

Reach is above the last Left bank meander, in the lower pasture, on Big Warrior Creek. Photo is taken from inside the easement looking upstream. This is series number 3 from the BWC reference photos.



MVC-005S, AH&W 98-12-9



DSC00248, 3/1/30

Reach below the high clay bank, in the lower pasture, on Big Warrior Creek. Photo is taken from the top of the bank looking downstream. This is series number 7 from the BWC reference photos.



MVC-004S, AH&W 98-12-9



05000040 3/1/30

Reach showing the high clay bank and above, in the lower pasture, on Big Warrior Creek. Photo is taken from the top of the bank looking upstream. This is series 8 from the BWC reference photos.



MVC-007S, AH&W 98-12-9



DSC00249, 3/1/30

Bend at the end of the middle pasture, on Big Warrior Creek. Photo is taken looking downstream from just above the bend. This is series number 13 from the BWC reference photos.



MVC-002S, AH&W 98-12-9



DSC00256, 3/1/30

Reach is in the middle of the middle pasture, on Big Warrior Creek. Photo is taken from a point bar looking upstream. This is series number 15 from the BWC reference photos.





DSC00258, 3/1/30

Reach below the Feed Barn, in the middle pasture, on Big Warrior Creek. Photo is taken from the property line survey point looking downstream. This is series number 17 from the BWC reference photos.







DSC00266, 3/1/30

Reach above the bridge in feedlot, on Big Warrior Creek. Photo is taken from the left bank just above the first sycamore, looking downstream to bridge. This is series number 24 from the BWC reference photos.



MVC-011F, AH&W 01-8-01



DSC00266, 3/1/30

Reach is in the middle of the feedlot, on Big Warrior Creek. Photo is taken from the right bank, just below survey point 1A44, looking upstream. This is series number 27 from the BWC reference photos.





DSC00266, 3/1/30

Reach is in the middle of the feedlot, on Big Warrior Creek. Photo is taken from the mid-channel, at the old cross-fence just below survey point 1A45 looking downstream. This is series number 28 from the BWC reference photos.



MVC-009S, AH&W 98-12-9



DSC00273, 3/1/30

Reach is in the upper end of the feedlot, on Big Warrior Creek. Photo is from the left bank, just above the old cross-fence at survey point 1A45 looking downstream. This is series 30 from the BWC reference photos.



MVC-0012S, AH&W 98-12-9



DSC00293, 3/1AA

Reach is in the middle of the upper pasture, on Big Warrior Creek. Photo is taken from the right ben's just below s.p. 1A65 looking downstream to eroding clay ben's area. This is series 52 from the BWC reference photos.



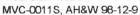
MVC-0013S, AH&W 98-12-9



DSC00290, 3/1/30

Reach is in the middle of the upper pasture, on Big Warrior Creek. Photo is taken from the right bank just below survey point 1A63 looking upstream to site of old headcut area. This is series number 49 from the BWC reference photos.







DSC00298, 3/1/30

Reach is at the upper end of the upper pasture, on Big Warrior Creek. Photo is taken from the left bank looking downstream to the single locust tree and cross-vane. This is series 58 from the BWC reference photos.

PEBBLE COUNT INFORMATION

	. 4				/1		<u></u>					ノ.	T .2		L	. .	Τ,	11		J.	T./	LL.	A T			1		/ 1
17		sample	WCOM	%0	1%	2%	11%	21%	78%	35%	38%	41%	46%	52%	61%	73%	87%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	
PEBBLE COUNT	5/7/2001	BWC bar sample	ITEM %	%0	1%	4%	%9	10%	8%	%9	2%	3%	2%	%9	10%	12%	14%	13%	%0	% 0	% 0	% 0	%0	%0	% 0	%0	%0	
3d	Date:	Reach:	# TOT	35	100	438	786	1237	941	789	303	383	561	741	1173	1515	1697	1553				,						12260
INT		pave.	WCOW	%0	%0	2%	2%	%6	12%	14%	16%	18%	23%	30%	46%	68%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	
PEBBLE COUNT	Date: 5/7/2001	BWC subpave.	ITEM %	%0	%0	%1	%E	4%	3%	3%	2%	7%	4%	8%	16%	21%	32%	%0	%0	%0	%0	%0	%0	%0	%0	%0	%0	
34	Date:	Reach:	TOT #	8	12	39	118	150	108		64	87	155	282	282		1188											3709
NT		ble count	% CUM	%2	13%	33%	38%	37%	37%	38%	41%	43%	20%	28%	%69	74%	82%	%68	81%	%66	%66	100%	100%	100%	100%	100%	100%	
PEBBLE COUNT		BWC pebble	ITEM %	6.8%	5.8%	20.4%	2.9%	1.0%	%0.0	1.0%	2.8%	1.9%	7.8%	8.7%	9.7%	4.9%	7.8%	7.8%	7.8%	1.9%	%0.0	1.0%	0.0%	0.0%	%0.0	0.0%	%0.0	
ā	Date:	Reach:	# TOT	7	9	21	3	1		1	3	2	8	8	10	5	8	8	8	2		1		,				103
			PARTICLE COUNT																							And the second s		TOTALS:
				S/C	S	Α	Z	D	တ		9	2	. V	^	Е		S		၁	0	8	٦	В	٦	۵	ď	10000 ВЕDROCK	
				0.062	0.125	0.25	0.5	1	2	4	5.7	8	11.3	16	22.8	32	45	64	90	128	180	258	362	512	1024	2048	10000	
			MILLIMETER	< .062	.062125	.12525	.2550	.50 - 1.0	1-2	2-4	4 - 5.7	5.7 - 8	8 - 11.3	11.3 - 16	18 - 22.8	22.6 - 32	32 - 45	45 - 64	64 - 90	90 - 128	128 - 180	180 - 256	256 - 362	362 - 512	512-1024	1024 - 2048		
	Site:	Party:	PARTICLE	Silt/Clay	Very Fine	Fine	Medium	Coarse	Very Coarse	Very Fine	Fine	Fine	Medium	Medium	Coarse	Coarse	Very Coarse	Very Coarse	Small	Small	Large	Large	Small	Small	Medium	Lrg-Vry Lrg	Bedrock	

Channel Particle Sizes (mm	$\overline{}$
cle	mm
cle	$\overline{}$
Channel Particle	Sizes
Channel Particle	4)
Channel Particl	. •
Channel Partic	~
Channel Parti	•
Channel Part	.=
Channel Page	ਢ
Channel Pa	~
Channel F	~
Channel	2
Channel	
Channe	75
Chann	\mathbf{z}
Chan	⋤
Cha	⊂
Š	⋥
Ü	~~
O	ټکہ
$\mathbf{\mathcal{I}}$	r
	$\mathbf{\mathcal{I}}$

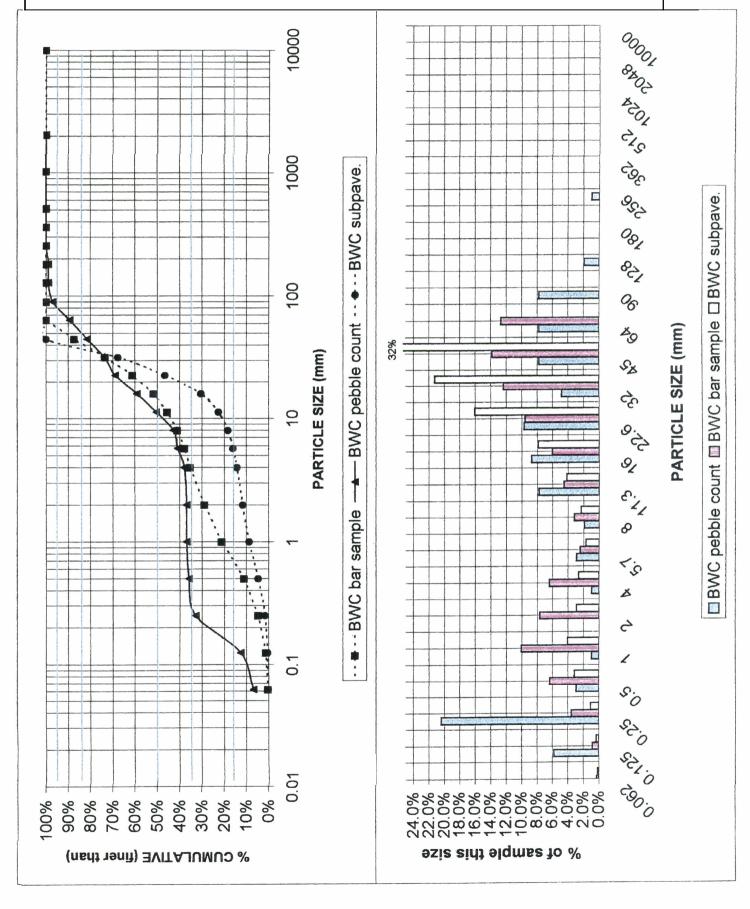
	mont					,	
	Cuhnawannant	D16	D35	D 50	D84	D95	
<u></u>					_		
CHAINTEI F ALUCIC SIZES (IIIII)	ıt:	0.13	0.28	11.3	20	08	
Cilainici r a	Pebble Count:	D16	D35	D50	D84	D95	

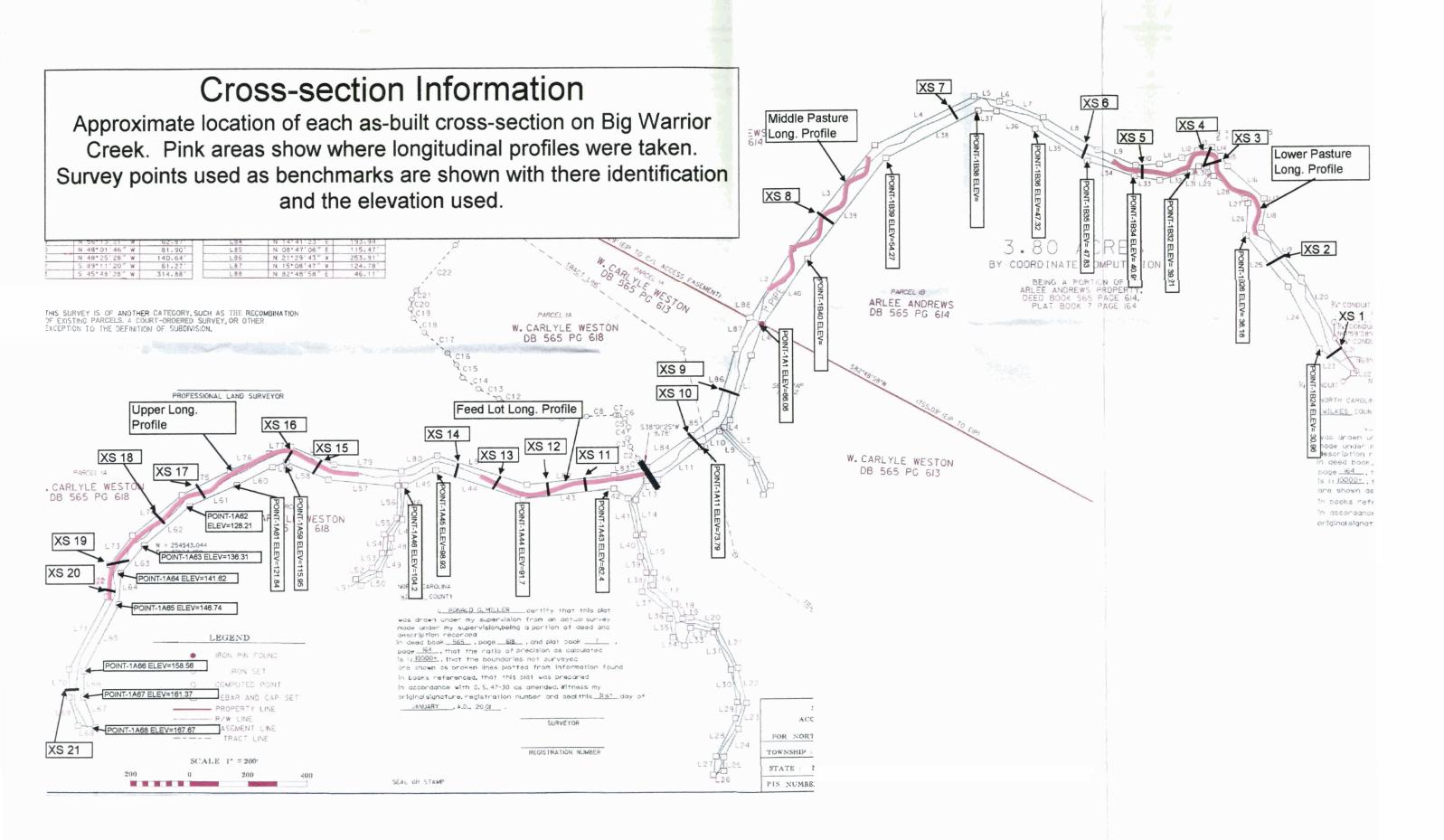
ple:	0.75	
Bar Sam	D16	
		-

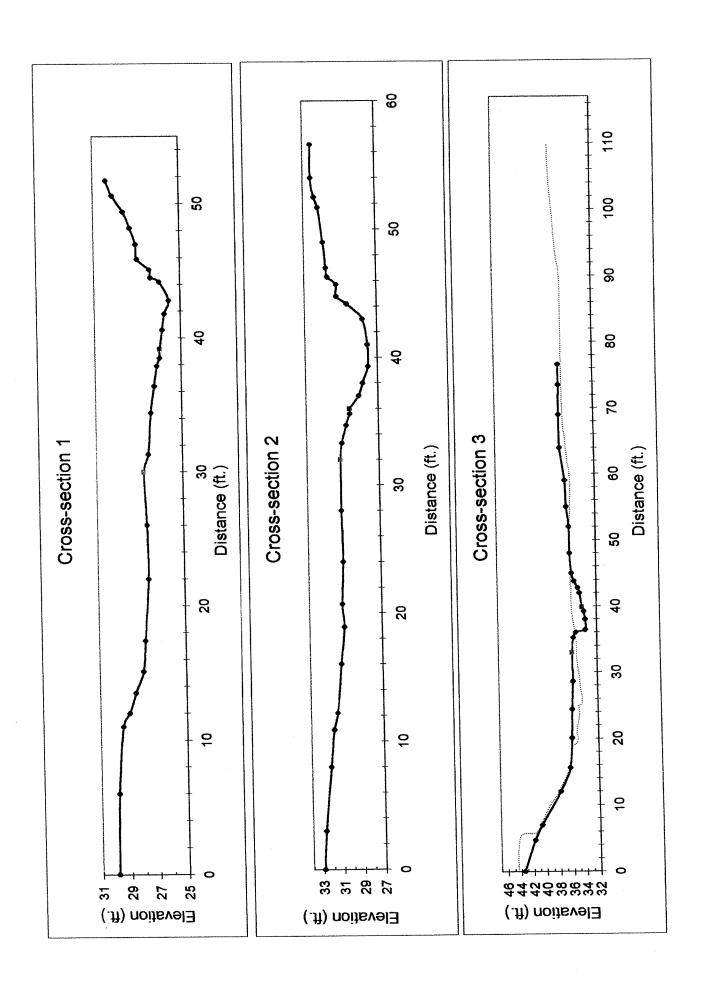
15.5	40	55
D50	D84	D95

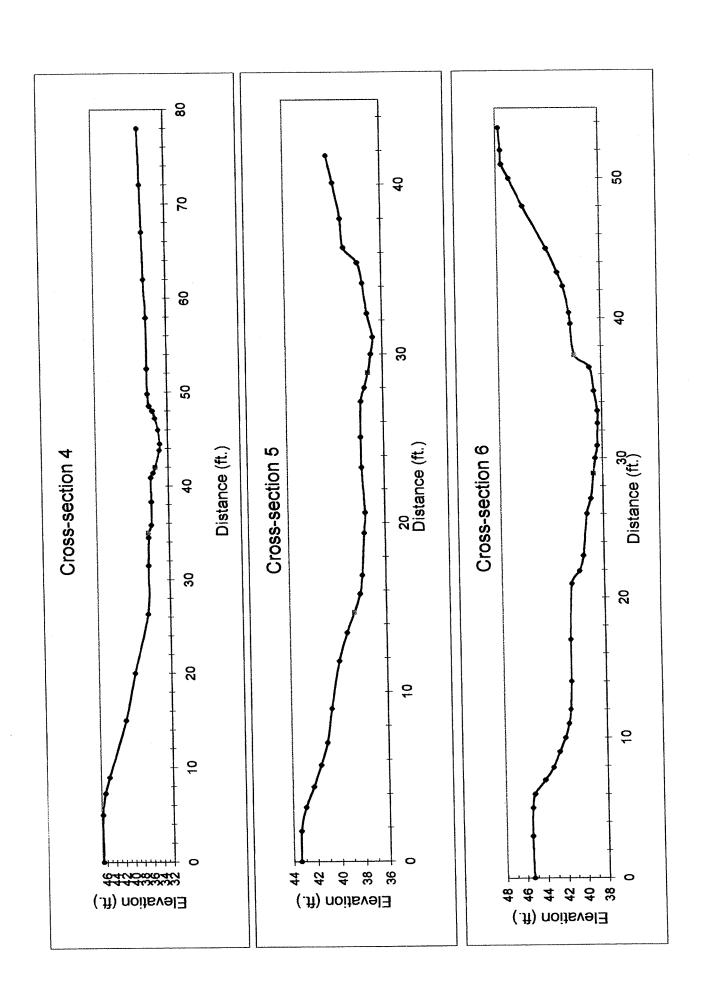
(
(ww)
Bar (
\mathbf{j}_0
Toe
ze at
st Size
rges

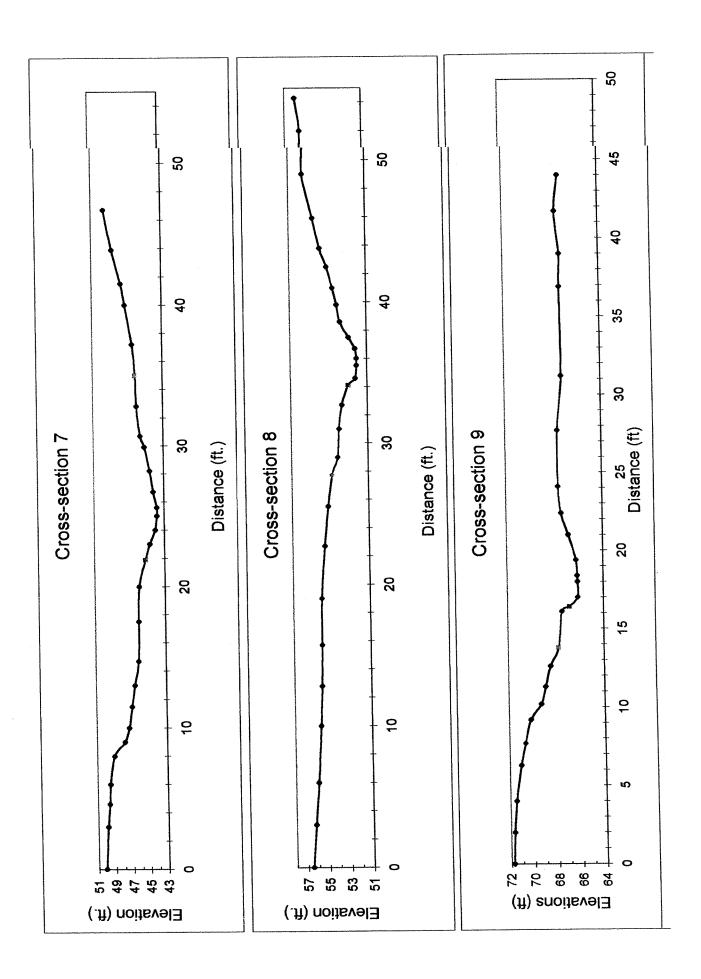
PEBBLE COUNT INFORMATION

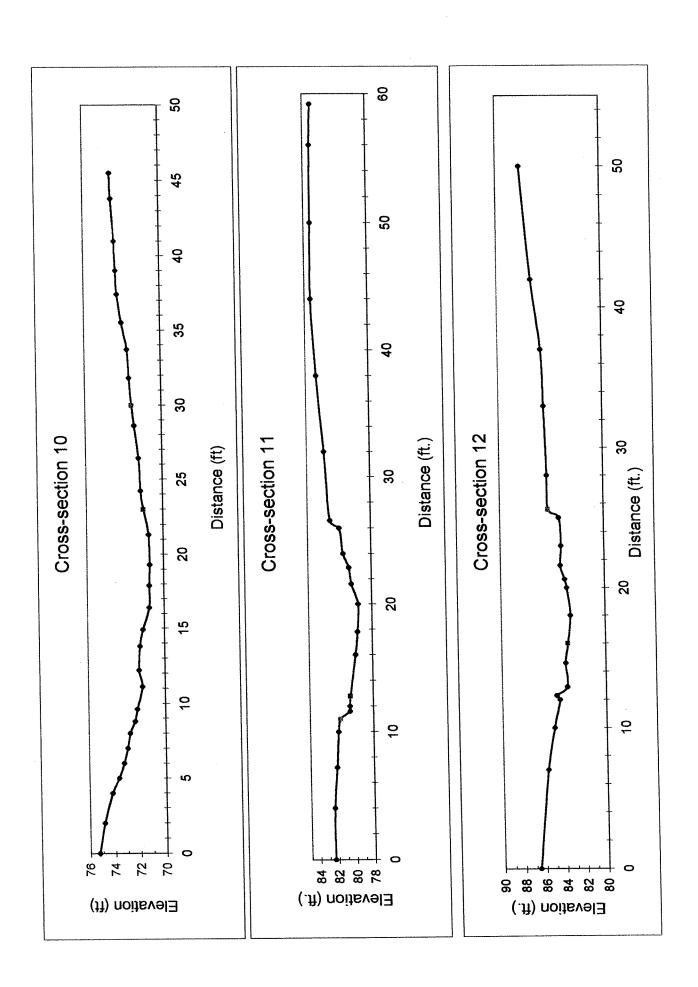




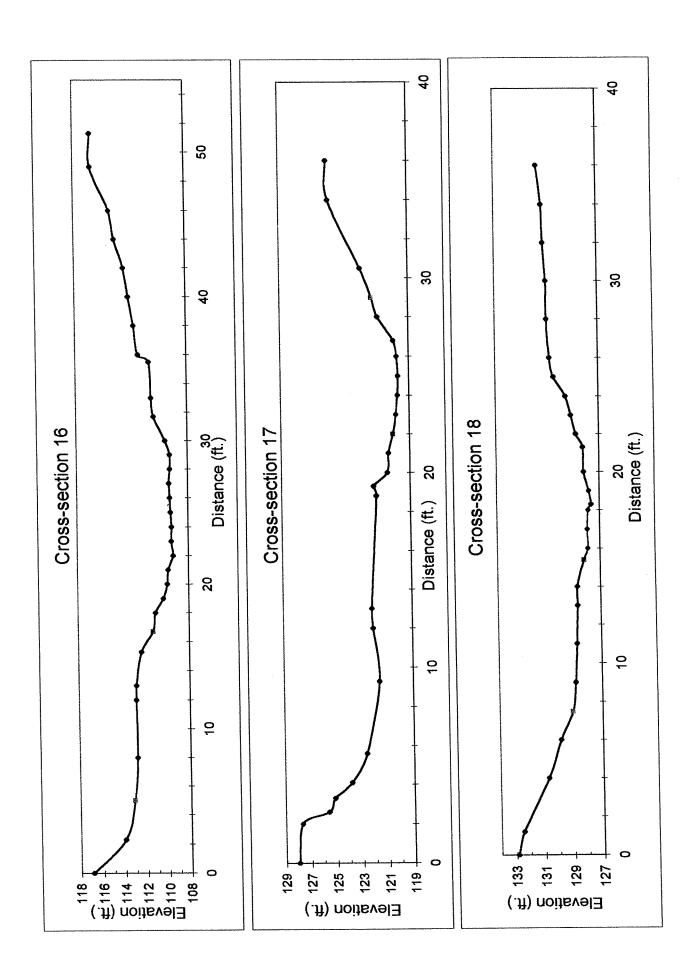


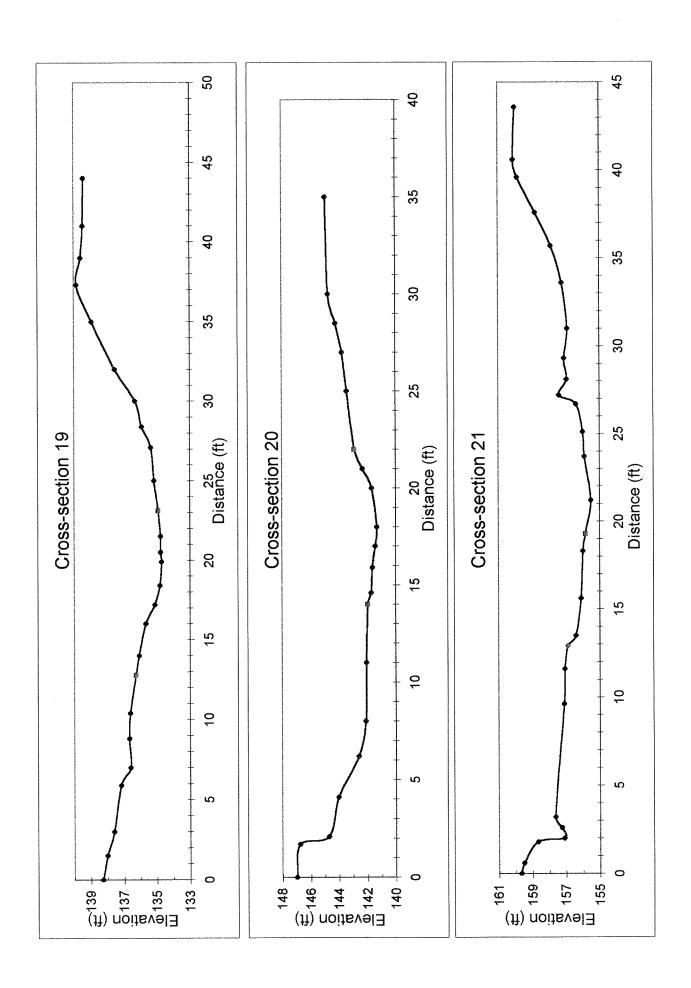












Longitudinal Profile Information for Upper Pasture

			1		below the center rock(rebar on the RB marks beginning). Long Pro. Starts on 507" on total channel length See other notes at bottom.	below the center rock(reba See other notes at bottom.	9		1 /6	5	arts on 507	Citora	annel leng		SE SE	Г	RIFFLE-POOI	! !		
Thal. Thal. Elev	it, Thal. Thal. Elev	Thal. Thal. Elev	Elev	slope	Н	W.S. W.	S. elev.	slope	BF	BF Elev.			T.B. elev.	П	pool niffe		H. riffle-L	R:P	TB-Thal B	Bkf-W.S.
0 26 5.85 141.75	26 5.85 141.75	5.85 141.75	141.75	1	-	4.71		0.0050	3.75	143.85		0.048	147.552	0.0397	2.1		28	83	5.802	96.0
147.6 26 55 5.09 142.51 0.03	55 5.09 142.51 2 8 85 140 95	5.09 142.51 8 85 140.95	142.51	-		8 25	142.76	0.0258	3.75	143.85	0.1	3 99	143.61	0.0000	1	1.34	/6		2.66	0.68
83 4 8.99 138.61	4 8.99 138.61	8.99 138.61	138.61	1 1		7.53		-0.0025	6.58	141.02	0.0	3.89	143.61	0.0500	2.41	H	4	28	S	0.95
50 7.62	50 7.62 139.98	7.62 139.98	139.98	- }		7.52	١,	0.0172	6.58	141.02	500	4.19	143.41	0.0256	+	104	54		3.43	0.94
141 6 10.43 137.17	6 10.43 137.17	10.43 137.17	137.17	1	-	9.81	137.79	0.0000	7.97	139.63	0.0	5.47	142.13	0.0000	2.46	-	11	101	4.96	1.84
147 5 10.87 136.73	5 10.87 136.73	10.87 136.73	136.73	1	-	9.81	1	0.0120	78.7	139.63	0.1	5.47	142.13	0.1700		-	-		5.4	1.84
152 38 10.21	38 10.21 137.39	10.21 137.39	137.39	1		9.87		0.0581	9.34	138.28	0.0	6.32	141.28	0.0518	7	0.87	8		3.89	0.53
190 50 12.54 135.06 240 2 5 35 132.78	50 12.54 135.06	12.54 135.06 5 35 137.78	135.U5			5 26	132.6	0.0546	3.85	134 78	5 6	27	135.43	0,000	T	+	1	\downarrow	2.65	1,41
242 6 6.58 131.55	6 6.58 131.55	6.58 131.55	131,55	1		6.15		0.0100	5.38	132.75	0.0	27	135.43	0.0000	1.2	H	1	35	3.88	0.77
248 5 7.13 131	5 7.13 131	7.13 131	131	1		6.21		0.0020	5.38	132.75	0.0	2.7	135.43	0.000.0		H			4.43	0.83
253 23	23 6.58 131.55	6.58 131.55	131.55	1		6.22		0.0013	5.08	133.05	0.0	2.7	135.43	-0.0304		1.5	24	4	3.88	1,14
276 1 6.62 131.51	1 6.62 131.51	6.62 131.51	131.51	11		6.25	1 1	1.4700	5.72	132.41	0.0	2	136.13	0.000	1	+	\dashv		4.62	0.53
277 16 9.65 128.48	16 9.65 128.48	9.65 128.48	128.48			7.72		0.0044	6.94	131.19	0.0	2	136.13	0.1781	2.71		16	62	7.85	0.78
293 45 8.1 130.03	45 8.1 130.03	8.1 130.03	130.03			7.79		0.0151	6.94	131.19	0.0	4.85	133.28	0.0664		1,16	46	9	3,25	0.85
338 1 8.97	1 8.97 129.16	8.97 129.16	129.16			8.47	ŧ	1.0100	7.84	130.29	0.0	7.84	130.29	0.6000					1.13	0.63
339 11 10.32 127.81	11 10.32 127.81	10.32 127.81	127.81	1		9.48	Į.	0.0000	8.44	129.69	0.0	8.44	129.69	0.000.0	1.88		23	87	1.88	1.04
350 12 10 85 127 48	12 10 85 127 48	10.85 127.48	127 48	1		9.48	}	0.0075	8 44	129.69	0.0	8.44	129.69	-0.0008	T	-	-		2.21	1.04
387 R1 108 13	R1 40 128 13	10 128 13	128 13	1		0.57	1	0,000,0	8 43	129.7	00	8.43	129.7	0.0179	İ	1.57	84	-	1.57	1.14
2 40 40 40 40 40 40 40 40 40 40 40 40 40	2 40 40 427 74	40 40 407 74	127.13	1		10.00		3400	0 52	128 R1	000	0 52	128 R1	0000	T	-			a	0.54
10.44	0 44 59 479 55	17.72 12.7.7	120 00	1	1	1000		0000	0.02	120.02	300	0.52	128 81	2000	900	ł	á	181	20.0	1 47
420	0 1,30 1,20,33	1.00 1.00.10	106 13	1		10.00		0.0000	0.02	128 84		0 53	128 81	0.1375	3	T	1		2 48	1 47
454 6 120.15	77 44 4 478 73	44.4 4.78.72	126.13	1		11.05		0.0073	40.82	127.51	2 5	10 62	127 51	0.0180	f	0 7B	185		0.78	0.43
27.021 4.11 77 52.00	27 77 72 00	44.07	432 00	l		13.67		0,000	12.02	125.02	-	11 95	120 20	0.050			-		CF C	27.0
17.41 10 011	1 0 04 120.00	0 04 420 00	120.00	1	1	0.77	1	00890	1000	124 44	3 0	7 01	124 11	0000	T	$\frac{1}{1}$	_	Ţ	- 3	80
0000011 10000	0.021 120.00	07.7	140 33	1	1	2	1	00000	7 0.1	124 14	200	7 01	121 11	0000	1 70	-	18	8	1 79	1.5
000	40 40 65 410 97	40.02	140 97	1	ı	270	140 64	00000	7 0.4	124 13		7 0	121	0.0000	+	l		3	27.4	5
1000 11000	1000 4400	10.00	140.5	1	1	200	1	0.0020	OP O	120 54	1	8 48	120 54	0.0101	t	134	47	_	134	10
2 10 00 118 04	2 10.08 118.04	10.08 118.04	118 04		1	10.72	1183	0 2000	10.24	118 78	0	932	119.7	0.1900	t	-	-		1.88	0.48
200 11 00 01 1 10.01	10.00	12 00 118 03	118 02	1		11 32	ł	00000	0 00	110 13	36	0 80	110 13		20	-	18	214	22	1.4
12 42 43 64 44 44	12 12 12 12 12 12 12	12 55 110.00	148.47	1	-	44 32	1	0,000	080	110 13	000	08 0	110 12	a nan	t	+	-		2.86	1 43
36 744 74 44 20	101 14 00 14 00	14.00 110.77	147.05	1	+	11 20	1	2420	10.00	418 34	200	10 89	119 34	0.0185	Ī	000	196	-	00 0	c
20,711 (2.11) 20 000	10371 1031 70	100,711	17.30	1	+	1.30	1	0.0217	2000	110.04		10.00	110 01	0000	1	90.0	1		1 75	1
111 13.76 113.24	111 13.76 113.24	13.76 115.24	10.24	1	Ţ	13.10	i	0.0234	3 5	142 24	- 0	1 03	443 34	2000	\dagger	ł	+	1	200	1
881 3 8.93 112.3	3 8.93 112.3	8.83 112.3	112.3	-1	1	20.00	112.0	0.0000	78.7	13.31	23 6	78.7	2007	0.000	1 00	+	ç	*	9	i c
9.00 000 000	18 9.0	9.0	11.03	1	1	0.00	1	0.0132	7 14	13.51	36	7 1.7	144.00	0.0454		4 82	200		18	7
905 20 6.90 112.27	77.71 08.90 77	0.90 112.27	12.21	1	1	0.00	1	10000	***	20.7		1 7	443.05	0000	T	1	1		1 14	000
900	00.111 00.01	9.00	0000	1	T	40.0		0000	1	412 02	200	5 4 4	112 82	2000	2 43	+	27	7	243	17
25.01 10.02 20 10.02 A	4 44 83 400 4	44 83 400 4	4004	1	T	10.01	1	0.0000	B 41	112 82	S	8.41	112 82	0.0246		-	-		3.42	,
959 48	46 10.61 110.62	10.61 110.62	110.62	1	1-	10.24	110.99	0.0191	6	112.23	0.0	6	112.23	0.0204		1.61	48	80	1.81	1.2
1005 2 11.31 109.92	2 11.31 109.92	11.31 109.92	109.92	1	1	11.12		0.4400	9.94	111.29	0.0	9.94	111.29	0.0000		_			1.37	1.18
1007 15 13.54 107.69	15 13.54 107.69	13.54 107.69	107.69	1	_	12	•	0.0060	9.94	111.29	0.0	9.94	111.29	0,0193	3.6		15	57	3.6	2.0
1022 40 12.38 108.85	40 12.38 108.85	12.38 108.85	108.85		М	12.09		0.0297	10.23	111	0.1	10.23	111	0.0422		2,15	5	2	2.15	1.86
1062 2 13.68	2 13.68 107.55	13.68 107.55	107.55			13.28	107.95	0.5800	11.92	109.31	0.0	11.92	109.31	0.000	1	+	1		1.76	1.36
1064 16 15.51 105.72	16 15.51 105.72	15.51 105.72	105.72	- 1	1	14.4	- 1	0.0019	11.92	109.31	0.1	11.92	109.31	0.1175	3.59	+	18	¥	3.59	2.48
1080 24 14.79	24 14.79 106.44	14.79 106.44	106.44	- 1	7	14.43	106.8	0.0367	13.8	107.43	0.0	13.8	107.43	0.0242		0.99	23		0.99	0.8
1104 1 15.6 105.83	1 15.6 105.83	15.6 105.63	105.83		7	15.31	105.92	1.3600	14.38	108.85	00	14.38	108.85	0.0800	1	+	-	1	1.22	0.93
1105 12 13.94 102.79	12 13.94 102.79	13.94 102.79	102.79	1	7	12.17	- 6	0.0108	96.6	108.77	0.1	9.8	106.77	0.1458	3.98	+	12	85	3.98	2.21
1117 48 12.85	48 12.85 104.08	12.85 104.08	104.08	١	1	12.3		0.0142	11.71	105.02	0.0	11.71	105.02	0.0085	1	0.94	<u>2</u>	†	0.84	CO
1165 2 13.3 103.43	2 13.3 103.43	13.3 103.43	103.43	- 1	7	12.98		0.4000	12.12	104.61	000	12.12	104.61	0.0000	c,	+	- ;	1	1.18	0.88
1167 16 14.85	16 14.85 101.88	14.85 101.88	101.88	1	8	13.78	102.95	0.0031	12.12	104.61	0.0	12.12	104.61	0.0594	2.73	+	10	1	2./3	9.0
1183 14.13	14.13				1	13.83	102.9	1	13.07	103.86	1	13.07	103.66		1	1.06	$\frac{1}{1}$		90.	0.7
				_	1	4	1	-	1	-	T	1		Avarage	90	1 27 1	17 5 BR 0	9 90	1 08	131
חפנים חים חבנים מי מים מים מים מים מים	0.0120	0.0120	0.0120		244	0.0075	0.0075	0.0120	n 0046	0.0132				- Dai DAC			1	1	1221	
Pool slopes = 0.0050 -0.0025 0.0120 0.0120 0.	Ĺ	Ĺ	Ĺ	E S	Spread	0.0073	Avn Po	Ava Pool slanes	0.0040	2010.0										
Avg. Signed 17.5 Avg. Riffle langth	L	L	L	Riffle las	1	88.9	1 7 7 7	2000	,											
				ar sure	3	0,00														

distance = 1183
1st top of bank = 147.552
last top of bank = 113.86
143.892 difference from top to bottom of the valley cross-section at 853' on this long, pro., 52.8'us of point 1459 cross-section at 948' on this long, pro., 1.75' ds of point 1459 cross-section at 1042.3' on this long, pro., 107' ds of point 1459 & 53' us of 1458 0.0371 Valley Slope = 1183 142.89 102.9 39.99 difference from top to bottom of the valley Water Surface Slope = 0.0338

min 1.88 0.94 12 25 41 0.94 0.59 max 3.98 2.15 27 196 75 3.99 2.49

Range:

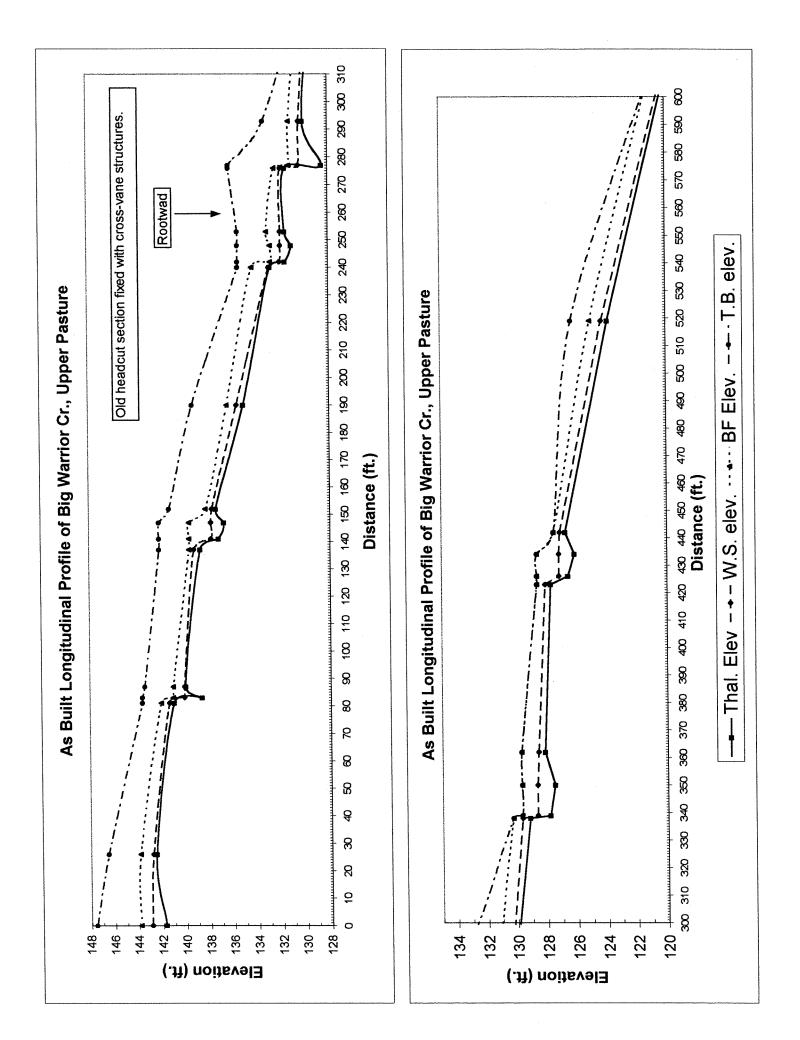
Valley slope from head of 1st top of bank to last

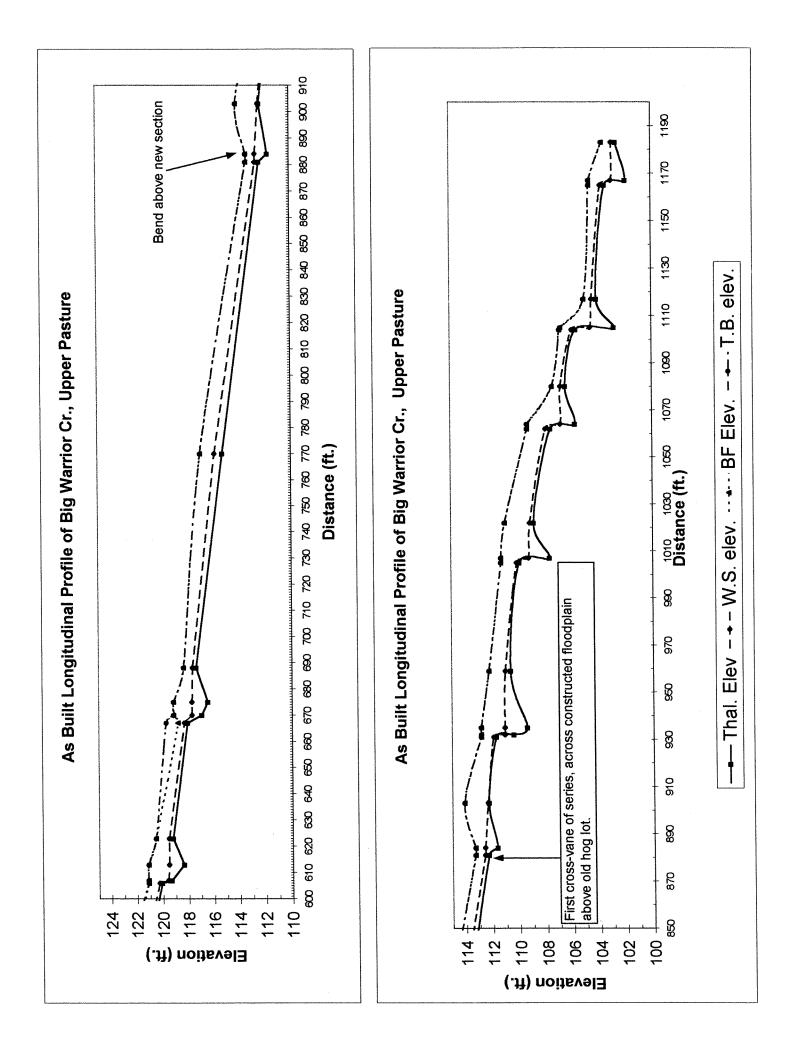
Water surface slope from head of 1st riffle to bottom of last pool

distance = top ==

79%

0 on this long Pro. Falls at 507' on total channel length 93' on this long Pro. Falls at 600' on total channel length 392' on this knog pro. Falls at 900' on total channel length. 691' on this long pro. Falls at 1200' on total channel length. 984' on this long pro. Falls at 1500' on total channel length.





Longitudinal Profile Information in Feed Lot

	Bkf-W.S.	0.81	0.68	1.84	1.95	0.89	0.92	1.13	1.45	1.03	1.3	2.26	2.79	1.2	1.63	1.51	0.89	1.44	2.47	2.65	1.56	1.36	1.39	1.25	0.72			1.46				0.68	2./3
		1.98	0.92	2.31	2.94	1.14	1.33	1.35	2.03	1,7	1.79	3.67	4.46	1.59	1.85	3.05	1.26	1.87	3.87	4.21	1.93	1.52	2.26	1.62	1.33	-	-	2.17				0.92	48
	TB-Thai										-				3		-								-	-		95.5			-	+	4
,	ب ج			175		49			8	16	-	79	_	99	118	_	82	-	85		65	10		88	-	-		73.5 95			-	16	\dashv
	-L riffle-L			17						16	_	13	_	_	34				20			12		_	_			7			-	49	4
ZF.	e pool-L					.14			2.03	_	-			1.59			.26				1.93			1.62	-	-		1.60 18.				_	2.03 34
Dbkf	pool riffle			2.31		*			2.	1.7		3.67		 -	1.85		1.	-	3.87		1.	1.52	_	1.1	1.33	-	_	2.32 1.			ŀ		3.87 2.
	edols	0.0100	0.000.0	-0.0550	0.0733	0.0278	-0.0033	-0.0050	0.0268	-0.0162		-0.1767	0.1550	0.0312	0900.0	0.0325	0800	0.000	-0.0400	0.0641	0.0362	0.000.0	0.0350	0.0302				Average=				E	max
	١.	91.96 0.0	91.81 0.0	91.81 -0.	_	90.82 0.0	89.46 -0.				87.33 0.0	i i	87.86 0.	86.31 0.0			83.41 0.0	82.75 0.0		82.87 0.0	81.78 0.0	79.43 0.0		79.22 0.0	.53	0	0	Ave				ige:	
	T.B. elev	L				L																										Range:	
	Top bank	6.97	7.12	7.12	7.01	8.11	9.47	9.42	9.4	11.81	11.6	11.6	11.07	12.62	6.37	6.43	7.2	7.87	78.7	7.75	8.84	11.19	11.19	11.4	14.09								
	edols	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.0	0.0	0.0	0.1	0.1	0.0	0.1	0.0	0.0	0.0	0.1	0.2	0.0	0.0	0.2		0.0							
	BF Elev.	91.96	91.81	91.81	91.92	90.82	89.46	89.51	89.53	87.12	87.33	87.33	87.86	86.31	84.25	84.19	83.41	82.75	82.75	82.87	81.78	79.43	79.43	79.22	76.53	0	0						
	#	6.97	7.12	7.12	7.01	8.11	9.47	9.42	9.4	11.81	11.6	11.6	11.07	12.62	6.37	6.43	7.21	7.87	78.7	7.75	8.84	11.19	11.19	11.4	14.09					0.0038		OTAL	
je.	slope	0.0013	1,1600	0.0000	0.0027	0.0284	0.0107	0750	0.0221	0.0046	0.3200	0.000.0	-0.0040	0.0377	-0.0060	0.0067	0.0148	0.5150	0.0200	0.0000	0.0331	0.0050	0.0117	0.0243					0.0083	=edojs		590 =TOTAL	
ad of the pool under the bridge.	W.S. elev.	91.15 0	Ι.		<u> </u>	L	l		1	l	86.03	ı	1	1	82.62	,		81.31 0	1	<u> </u>	80.22 0	1	<u> </u>		75.81	0	0		0.0100	Avg. Pool slope=		75%	
apun jood	S. W.S.	l	7.8					10.55			12.9					7.94		9.31	L		10,4		12.58		14.81				J	0.0267			
ad of the	W.S.	L	-		-		-		-				_			L		-		_	-						_		0.0	= 0.0	th 73.5	h 441	
at the hea	slope	90.0-	1.39	0.26	0.05	0.03	0.00	0.17	0.02	-0.01	0.63	0.09	-0.13	0.04	0.13	-0.04	0.02	8	0.07	-0.07	0.03	0.12	-0.07	0.03					-0.002	fle slope	ffle leng	Total Riffle lengt	
	Thal Elev	86.68	90 89	89.5	88.98	89.68	88.13	88.16	87.5	85.42	85.54	83.66	83.4	84.72	82.4	81.14	82.15	80.88	78.88	78.66	79.85	77.91	77.17	77.6	75.2	0	o		0.0046	Avg. Riffle slope=	Avg. R	Total R	
	Thal	5	8.04	9.43	9.95	9.25	10.8	10.77	11.43	13.51	13.39	15.27	15.53	14.21	8 22	9 48	8.47	9.74	11.74	11 96	10.77	12.71	13.45	13.02	15.42		-		0.0013			19%	
L	Tot Dist	L .	-	2	15	49	15	4	8	13	3	3	10	99	10	24	82	2	6	17	99	9	9	68		0	0		Pool slopes= (<u></u>	18.7		
	H	0	15	16	18	33	88	97	101	191	204	207	210	220	286	296	320	402	404	407	424	489	495	501	590	_	-		Pool s	pe= 0	ngth	112 ngth	
	l enoth	1	32																										L	Avg. slope=	g. Pool let	Total Pool length 112	
	Ī	Ļ	386	986	986	386	386	1	1	38.6	986	986	986	386	6	6	906	╀	╀	+	906	906	906	90,6	90.62	_				<u> </u>	¥	Tot	
	Feature	Depth	to of xv	HOP	Denth	i di	Sin	to of J-h		HoP	top of xv	Hop	Denth	HOR	acH	Denth	I SE	top of xv	HOP	Denth	HOR	HoP	Depth	HoRi	요								

Longitudinal Profile Data Sheet for: As-built information on AH&W site.

Profile description: Feed Lot longitudinal profile starts at bridge and goes upstream 600. It begins at deepest part of pool in front of rootwad just over from ds end of feed trough. It goes ds to us side, middle of bridge, ending

239' on this F.L. Long. Profile falls at 2400' on the total channel length 536' on this F.L. Long. Profile falls at 2700' on the total channel length

Water Surface Slope = 0.0260

Cross-section #12 is located at 418.7 on the F.L. Long. Profile Cross-section #13 is located at 253' on the F.L. Long. Profile Cross-section #14 is located at 92.6' on the F.L. Long. Profile

76.53 15.43 difference from top to bottom of the valley

Valley Slope =

590 91.96

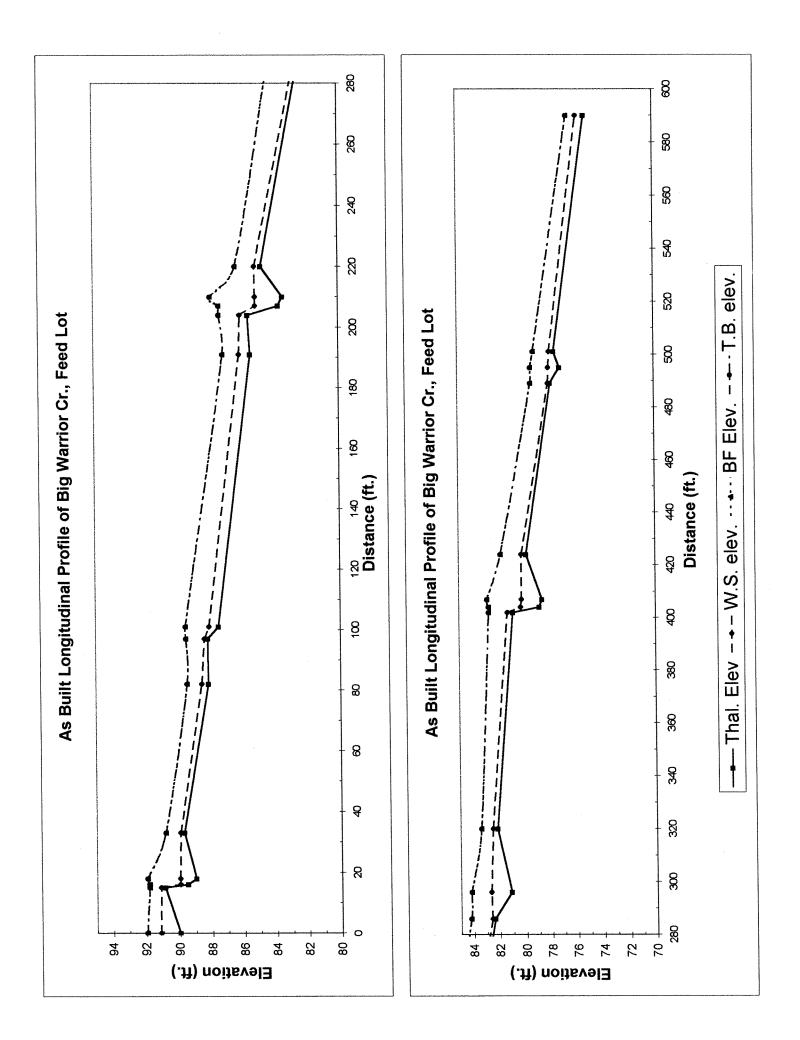
distance = 1st top of bank = last top of bank=

590 91.15 75.81 45.34 difference from top to bottom of the valley

Water surface slope from head of 1st riffle to bottom of last pool

distance == top == bottom ==

Valley slope from head of 1st top of bank to last



Longitudinal Profile Information for Middle Pasture

		Bkf-W.S.		1.09	0.68	0.81	0.91	0.7	0.92	0.78	0.95	1.12	1.29	1.18	1.31	1.31	1.09	1.18	₹	1.23	0.96	0.81	0.86	1.34	1.37	1.26	0.94	98.0	0.46	0.57	0.83	0.73	0.99			7 46	1.37
			1.36	2.1	0.98	1.38	1.6	1.12	1.38	2.27	1.35	1.62	2.42	1.56	1.91	2.31	1.59	1.57	1.75	1.54	1.26	1.86	1.29	1.97	2.47	1.7	1.34	1.51	1.6	0.39	1.24	1.68	1.62			000	2.47
		ا۔	-	8	1	\dashv	32	1	1	66	1	94			78		_	78			8	_	-	23	-	+	1	88	+				66.3			ç	98
		fle-L R	1	-	18		1	9	1		23			89	_		34			54		-	34	1		20	1	1	ļ	25	1	_	44.3			0,	2 88
	RIFFLE-POOL	pool-L riffle-L		12	1		13		1	9	1	26			44		-	24			56			14			1	53	1	1	1	_	22.0			5	54
	-		1.36		0.98			1.12			1.35		لـــــا	1.56			1.59			1.54			1.29				1.34			66.0			1.31				1.59
m 602'. oth	Ы	pool		2.1			1.6			2.27	_	1.62			1.91			1.57			1.26		Н	1.97		4		1,51	4	_	1.24		1,71				n 1.24 x 2.27
wnstrear marks bo		slope	0.000	0.0342	0,000	0.0500	0.0208	0.000	0.0450	0.0280	0.0175	-0.0240	0.0095	0.0163	-0.0200	0.0082	0.0350	0.0190	-0.0207	0.0241	0.0188	-0.0028	0.0129	0.0000	0.0350	0.0130	0.0154	0.0413	0.0010	0.0206	0.0500		Average=				min
ind goes do		T.B. elev.	60.72	60.72	60.31	60.31	60.16	59.89	59.89	59.71	59.43	58.4	58.52	58.32	57.21	57.33	57.02	55.83	55.64	55.93	54.63	54.48	54.53	54.09	54.09	53.81	53.38	52.98	52.65	52.63	51.6	51.4					Kange:
feed barn a downstrea		Top bank T	7.21	7.21	7.62	7.62	7.77	8.04	8.04	8.22	8.5	9.53	9.41	9.61	10.72	10.6	10.91	12.1	12.29	12	13.3	13.45	13.4	6.98	6.98	7.26	7.69	8.09	8.42	8.44	9.47	9.67			iovoš.	1	السب
te. Eudinal profile starts at 1st J-hook at end of cross-fence from feed barn and goes downstream 602' of the 1st J-hook vane and ends in deepest point of pool 602' downstream. Rebar marks both		_ edojs	0.0	0.1	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.0	0.0	0.2	0.0	0.1	0.2	0.0	-0.1	0.3	0.0	0.0	0.1	0.0	0.1	0.1	0.1	0.1	0.0	0.2	0.0			-0.0088			
d of cross-t	_	F Elev.	60.72	60.72	60.31	60.31	60.16	59.83	59.89	59.71	59.43	58.4	58.52	58.32	57.21	57.33	57.02	55.83	55.64	55.93	54.63	54.48	54.53	54.09	54.09	53.81	53.38	52.98	52.65	52.63	51.6	51.4		0.0131			
hook at encords in dee		BF BF	7.21	7.21	7.62	7.62	7.77	8.04	8.04	8.22	8.5	9.53	9.41	9.61	10.72	10.6	10.91	12.1	12.29	12	13.3	13.45	13.4	6.98	6.98	7.26	7.69	8.09	8.42	8.44	9.47	9.67		0.0000	0.0056		=TOTAL
ts at 1st J-		slope	0.0640	0.000.0	0.0087	0.0833	0.0046	0.0147	0.0100	0.0450	0.0203	0,0100	0.0043	0.0182	-0.0200	0.0024	0.0376	0,0010	-0.0043	0.0191	0.000	00000	0.0271	0.0050	0.0213	0.0033	0.0169	-0.0237	0.0062	0.0258	0.0250			-0.0016	=adols		548 =T
ofile star		١.	59.95	L	59.63	1	<u>L</u>	i	<u> </u>		ı	57.28 0.		57.14 0.	1	1	55.93	1	54.64 -0		1	į.	53.67 0	1	1				52.19 0.			50.67		-0.0088	Avg. Pool slope=		73%
udinal pr		W.S. elev			36							100										l												P			
	2	W.S.	7.98	8.3	8.8	8.43	8.68	8.74	8.96	0,	9.4	10.65	10	10.79	12.03	119	1	13.28	13.29	13.2	14.2	14.26	14.26	8.3	8.3	8.5	8.6	9.0	8.8	9.0	10.	10					388
heet for: As-built information on AH&W s Profile description: Middle Pasture longii Hearins on the too	ends of profile.	edojs	0.15	90.0-	0.03	0.12	-0.02	0.02	0.27	-0.06	0.02	0.14	-0.03	0.02	0.05	0.04	0.03	0.04	0.04	0.02	600	-0.03	0.03	0.08	90.0-	00.0	0.02	0.05		0.03	0.16			0.0450	Avg. Riffle slope=	Avg. Riffle length	(iffle length
scription:		Thal. Elev	59.36	58.62	59.33	58.93	58.56	58.77	58.51	57.44	58.08	56.78	56.1	56.76	55.3	55.02	55 43	54 26	53 89	54 39	53.37	52 62	53.24	52.12	51.62	52.11	52.04	51.47	51.05	51.64	50.36	49.72		0.0046	Avg. R	Avg. F	Total R
set for: A		Thal.	8.57	9.31	8.6	6	9.37	9.16	9.42	10.49	9.85	11.15	11 83	11.17	12 63	12.91	12.5	13 67	14 04	13.54	14.56	1531	14.69	8 95	9.45	8.96	9.03	9.6	10.02	9.43	10.71	11.35		0.0000			36%
Data She	1	Dist	2	12	15	8	13	15	4	10	29	2	21	88	G	38	34	9	14	5.4	80	ď	34	9	8	33	26	8	21	20	4			Pool slopes=	0.0154	22.0	
Profile		h Tot	0	5	17	33	32	48	63	67	77	38	41	162	5	986	274	308	318	333	386	700	412	446	452	460	493	519	527	548	298	602		Pool s	oe= 0	gth	198 ath
ngitudina		Length	L																																Avg. slope=	Avg. Pool length	Pool len
Γο		Ī		67 93	67.93	67 9	L	L	┸	┸	L	67.9	67.9	67.9	67.0	67.0	67.0	67.0	87.0	67.9	67.9	67.0	67 93	610	610	╀	╄	↓_	┞	61.07	61.0	61.07				Avg	Tota
		Feature	ton of .l-h	HoP&Den	HoRi	to not	HoP&Den	I SE	ton of .l-h	HoP&Dep	HOR	a o I	Denth	HOBI	aori	Denth	i i i	1001	Denth	ig G	a de	Denth	HOR	a H	Denth	HoRi-run	HoRi	모	Depth	구 전 기	HOF	Depth					

Cross-section #8 is located at 466.5 on the M.P. Long. Profile

51.4 9.32 difference from top to bottom of the valley

Valley Slope =

Valley slope from head of 1st top of bank to last

500 60.72

Valley distance = 1st top of bank = last top of bank=___

602 59.95 50.67 9.28 difference from top to bottom of the valley

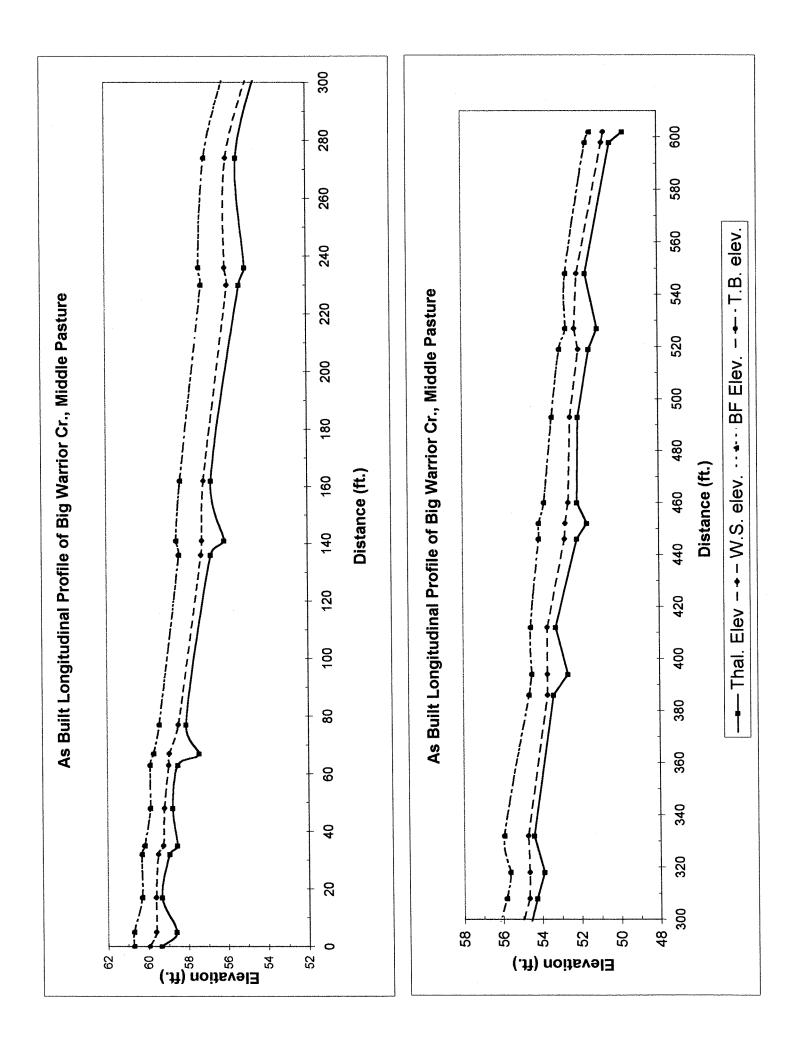
= mottog

Channel distance =

Water surface slope from head of 1st riffle to bottom of last pool

3624' to where the Middle Pasture Long. Profile begins on the total channel length

Water Surface Slope =



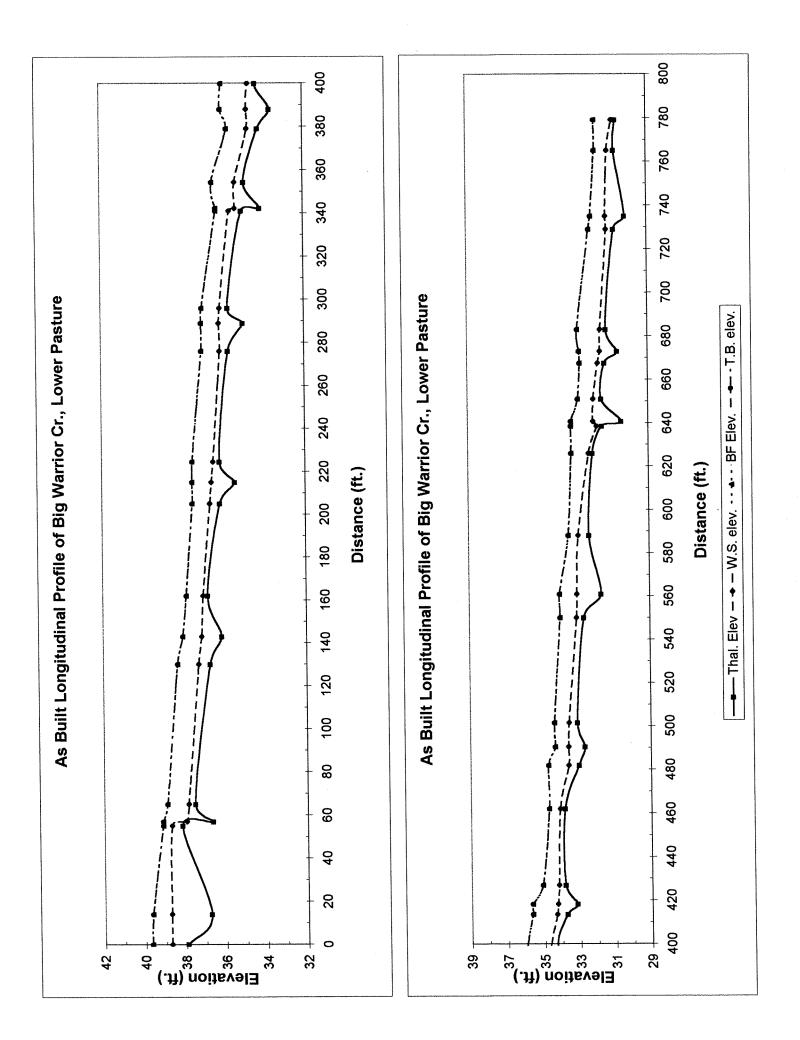
Longitudinal Profile Information for the Lower Pasture

	_	_																																													
	0.419	DKI-VV.O.	0 0	0.83	1 10	1.05	1.06	0.95	0.83	0.88	0.96	1.04	0.91	0.87	0.9	0.67	0.95	1.13	1.01	22.	1.32	1.35	1.41	0.91	0.62	1.14	0.75	0.82	0.91	0.96	0.55	0.97	1.42	1.24	, CO	1.02	1.26	0.97	0.84	0.71	0.97		0.98	0.4	1.4		
		10-1 ngi	9 5	7.81	2 49	1,38	1.63	1.94	1.07	1.37	2.11	1.35	1.31	2.06	1.28	1.26	2.17	1.58	1.54	2.41	1.67	1.93	2.49	1.27	0.89	1.7	1.65	1.28	1.34	2.3	1.15	1.18	1.73	2.79	7.52	2 42	1.59	1.38	6.1	1.09	1.17		1.66	6.0	2.9		
	ř	Ī	0.00	75.0	2.0	\dagger	75.0	-		71.0		-	65.0	1	+	38.0	+	1	34.5	-	1	68.5	1	+	1	0.89	+	1	88.5	1	1	+	29.0	+	0	0.10	-	-	\vdash	_	-	Н	60.8	29.0	88.5		
3	Ċ	TITIE-L K	1	1	+	65.0	Ľ		43.0	_		51.5		1	45.0	7	+	24.7	1		13.7		1	55.0	1		1	48.5		1	50.5	1	+	1	16.0	+	46.0	+	\vdash	14.0	-		9		65.0		
ב נ		Pool-L CIT	25.0	0	2.0	+	32.0	-		19.5		1	20.0	1	1	13.3	1	1	20.8	+	+	13.5	-	1	+	19.5	+	+	38.0	+	1	\dashv	12.5	+	- 1	0.0	1	36.0	\vdash	L		Н		-	55.0 6		
Γ	7	od a	1	+	+	14	L	H	1			1.4		1	1.3	+	+	1.6	+	1	1.7	1	1	1.3	1	-	1	1.3		-	1	1.2	1	+	5	\dagger	1.6	L	L		-	Н	1.3	\dashv	1.7 5		
i	≍г	000	+	6.2	2,5	1	l	1.9			2.1			2.1	1	1	2.2	1	1	2.4	1	1	2.5	1	1	1	1.7		1	2.3		1		2.8	1	ç	1	\dagger	1.9				2.3	1.7	2.9		
_	7	_	0.0021	62.00	0.0000	0.0207	0.0208	0.0100	0.0077	0.000.0	0.0021	0.0095	0.000.0	0.0043	0.0162	0.000.0	-0.0150	0.0296	-0.0322	0.0034	0.0234	0.000.0	0.0655	0.0111	-0.0010	0.0459	-0.0027	0.0076	-0.0018	0.0193	0.0053	0.0000	0.0000	0.0369	0.0073	CC00.0-	0.000	0.0167	0.0077	0.000.0			Average=	min	max		
		- 1.	_1	28.83			_	L								1	36.29	- 1	1	- 1	- 1	35.67		- 1	- 1	1	34.34	1	1	1	I	1	33.3	33.3	_1	37.8	32.93	32.22	32 12	31.89	31.89			Range:			
	ľ	-	7.01	20.	/0.7	78.7	8.34	8.61	8.8	9.13	9.13	9.15	9.64	9.64	9.67	10.4	10.4	10.22	10.95	10.66	10.7	11.02	11.02	11.59	11.98	11.96	12.35	12.32	12.69	12.67	7.8	8	8	8	8.38	8.0	8 30	80.0	9 18	9.41	9.41			-0.0008			
	ŀ		0.0	0.0	0.0	0.00	000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0			000	0.0				0.0114			
	4	- 1		1		38.12								37.05					35.74	I			Ц				34.34							33.3	32.92	32.8	32.03	30.00	32 12	31.89	31.89			0.0034			
before the rootwad and ends on the the J-hook	į	늅				/C./			L										10.95				11.02	11.59	11.98				12.69			8		ļ	8.38	8.5	0.47 20	200	9.00	9.41	9.41				0.0049		Ā
ds on the	rag as it crosses the vane, 35' ds of 1B26	in a	1	1		-		-	L	L						4															ຄ	00	8		72	8 0	2 0		3 2	99							779.0 =TOTAL
ad and er	the vane	slope .			- [0.0113	1		0.0088	1											7 0.0255										5 0.0163		8 -0.0818	- 1	. I.	8 0.0218		_L		L	L				Avg. Pool slope=		
the rootw	it crosses	W.S. elev			١	37.83			37.06									35.34																	32.05		31.00							0			61%
pool before	halwag as	W.S.	7.97	7.97	8.01	8.70 8.85	9.0	9.56	9.63	10.01	10.09	10.19	10.55	10.51	10.57	11.07	11.35	11.35	11.96	11.95	12.02	12.37	12.43	12.5	12.6	13.1	13.1	13.14	13.6	13.63	8.35	8.97	9.45	9.24	9.25	9.52	9.04	20.04	10.03	10 12	10.38			l°.	0.0148	39.5	473.4
head of the pool	vane in the thalw	edols	0.08	-0.03	0.77	50,0	200	0.04	0.01	0.07	-0.08	0.01	90.0	-0.11	0.02	0.70	-0.06	0.03	90.0	-0.06	0.04	0.12	-0.07	00.00	0.04	0.04	-0.04	0.01	0.09	-0.02	0.01	0.04	0.49	-0.11	0.0	0.13	97.00	500	2 5	0.01				0.0093	Avg. Riffle slope=	Avg. Riffle length 39.5	Total Riffle length 473.
	ı	Thal. Elev	37.92	36.74	38.16	30.03	36.70	36 14	36.82	36.19	35.45	36.19	35.74	34.99	35.74	35.03	34.12	34.89	34.2	33.62	34.32	33.74	33,18	33.83	33.82	33.03	32.69	33.09	32.69	31.72	32.35	32.12	31.59	30.51	31.6	31.41	24.05	20.10	30.04	30.8	30 72			0.0080	Avg. Ri	Avg. R	Total R
	1	- 1	8.77	9.95	8.53	00.00	0 0 0	10.55	9.87	10.5	11.24	10.5	10.95	11.7	10.95	11.66	12.57	11.8	12.49	13.07	12.37	12.95	13.51	12.86	12.87	13.66	14	13.6	14	14.97	8.95	9.18	9.71	10.79	9.7	9.89	10.5	3,30	2 20	10.5	10.58	2		0.0005	_		39%
		Tot. Dist.	14	41	7	χ	3 5	9	43	10	9.5	51.5	13	7	45	1.3	12	24.7	6	11.8	13.7	4.8	8.7	35	20	8.5	11	48.5	=	27	38	12.5	2.2	10.3	16.5	5.5	2 9	of G	0 0	14	F	Ī		Pool slopes=	0.0100	23.5	
	ł	Length	0	14	1 22	/c	3 5	143	162	205	215	224.5	276	289	296	341	342.3	354.3	379	388	399.8	413.5	418.3	427	462	482	490.5	501.5	550	561	588	929	638.5	640.7	651	667.5	6/3	2002	727	785	277			Poc	Avg. slope=	ool length	Total Pool length 305.6
		工	46.69	46.69	46.69	46.69	40.03	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	46.69	41.3	41.3	41.3	41.3	41.3	41.3	41.3	0.14	δ. 14 δ. 14	1 3	5 6	7		L	Æ	Avg. P.	Total P
		Feature	loP	epth	op/top xv	epth	200	hanth	i i i	dol	hepth	loRi	dop	epth	JoR.	-L dol/dol	epth	19Ri	do do)epth	양양	4oP)epth	JoRi	īŽ	g Q)epth	50Ri	PP	Septh	trun	원 장 한	lop/top xv	Septh	loRi	요	Septh	Ž,	100	i don	d-l do do	5 5					

ater surface slope from head of 1st riffle to bottom of last pool	Valley slope from head of 1st top of bank to last	pp of bank to last
distance = 779 top = 38.72 bottom = 30.92 7.80 difference from top to bottom of the valley	distance = 1st top of bank = last top of bank=_	590 39.68 31.89 7.79 difference from top to bottom of the valley Sinussity based on slope= 1.3186
Water Surface Slope = 0.0100	Valley Slope = 0.0132	

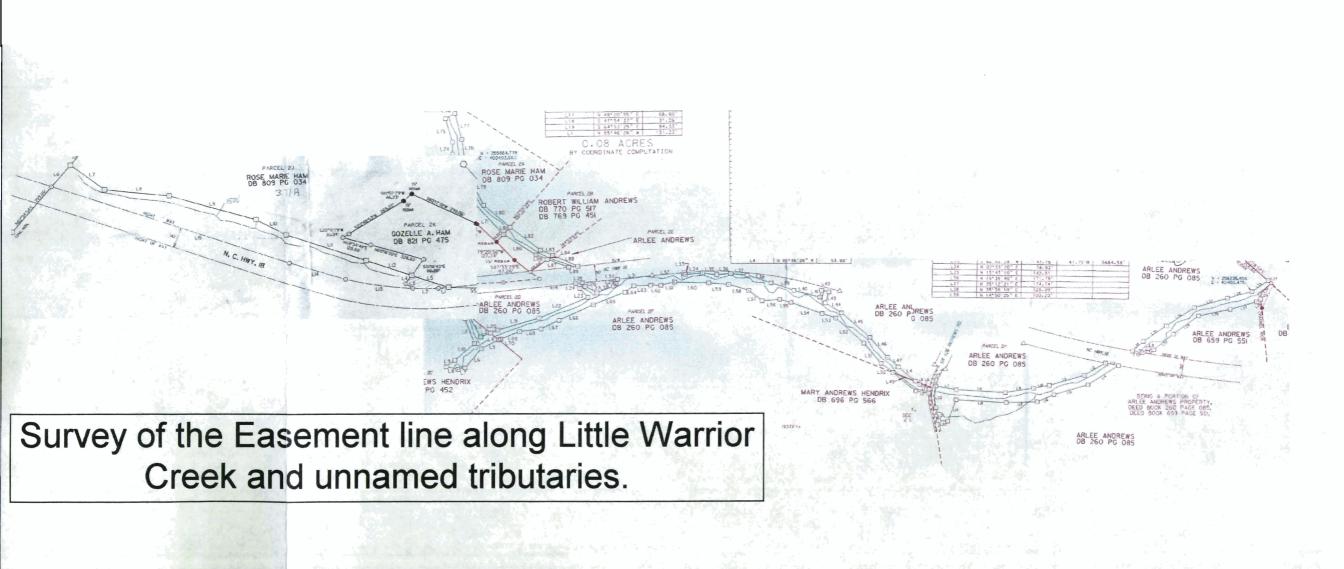
Longitudinal Profile Data Sheet for: As-built information on AH&W site.

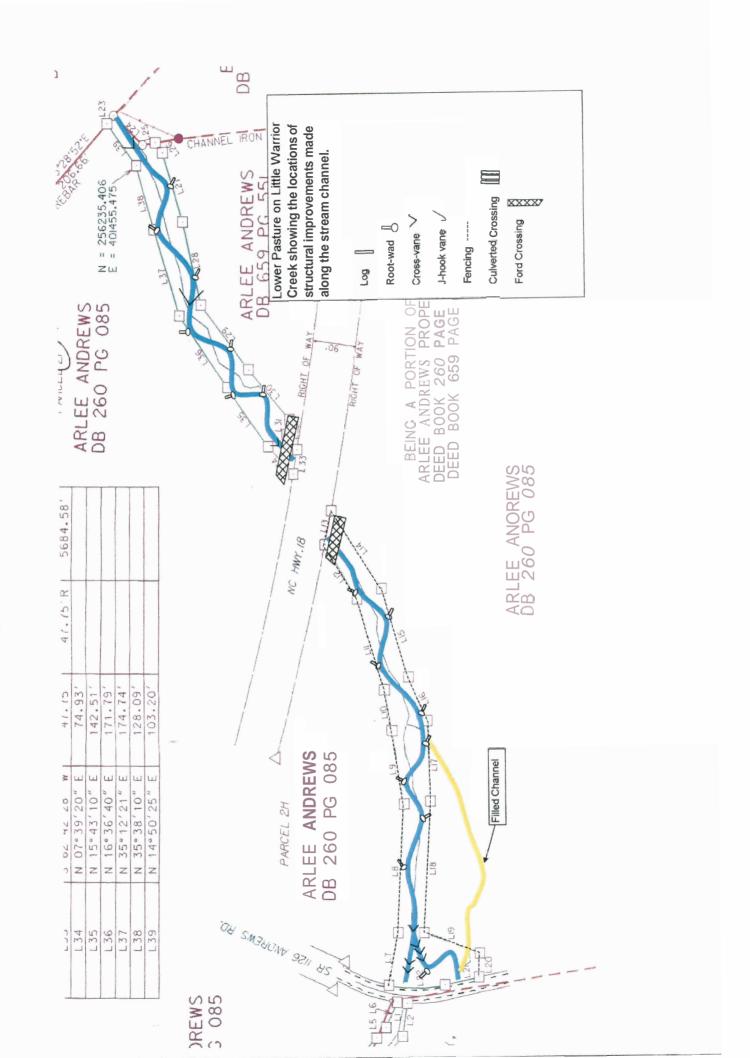
4oP&Dep

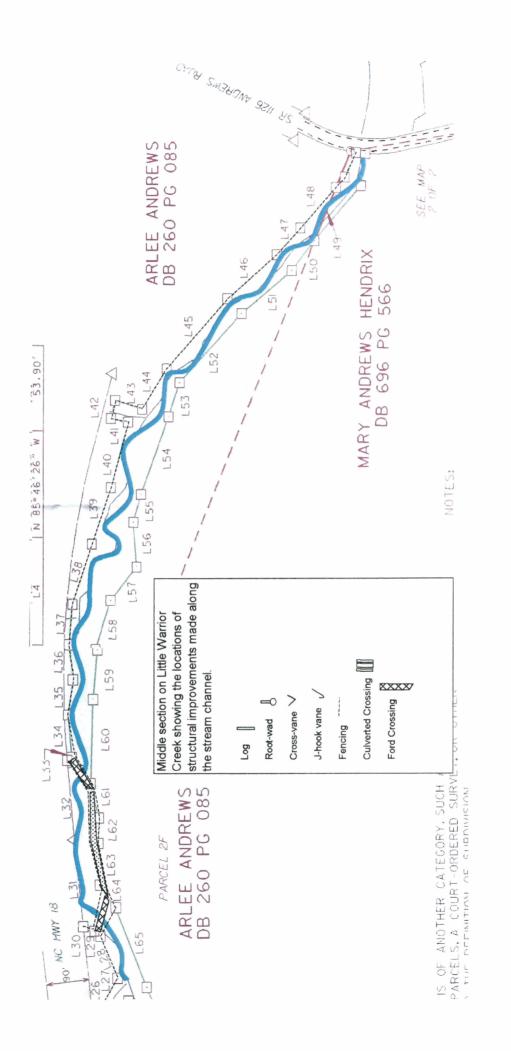


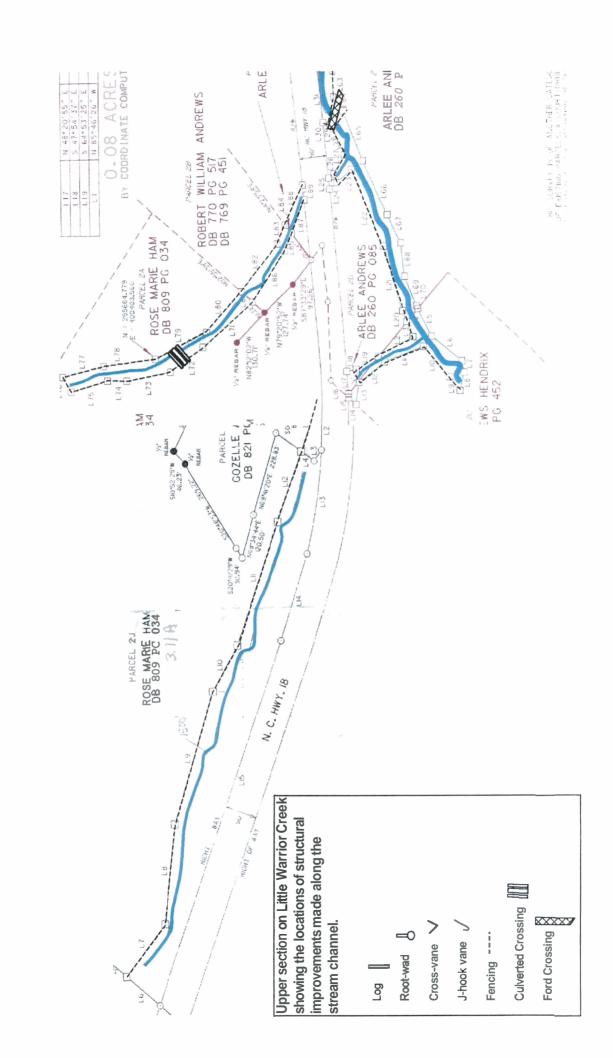
Little Warrior Creek As-built Stream Restoration Data

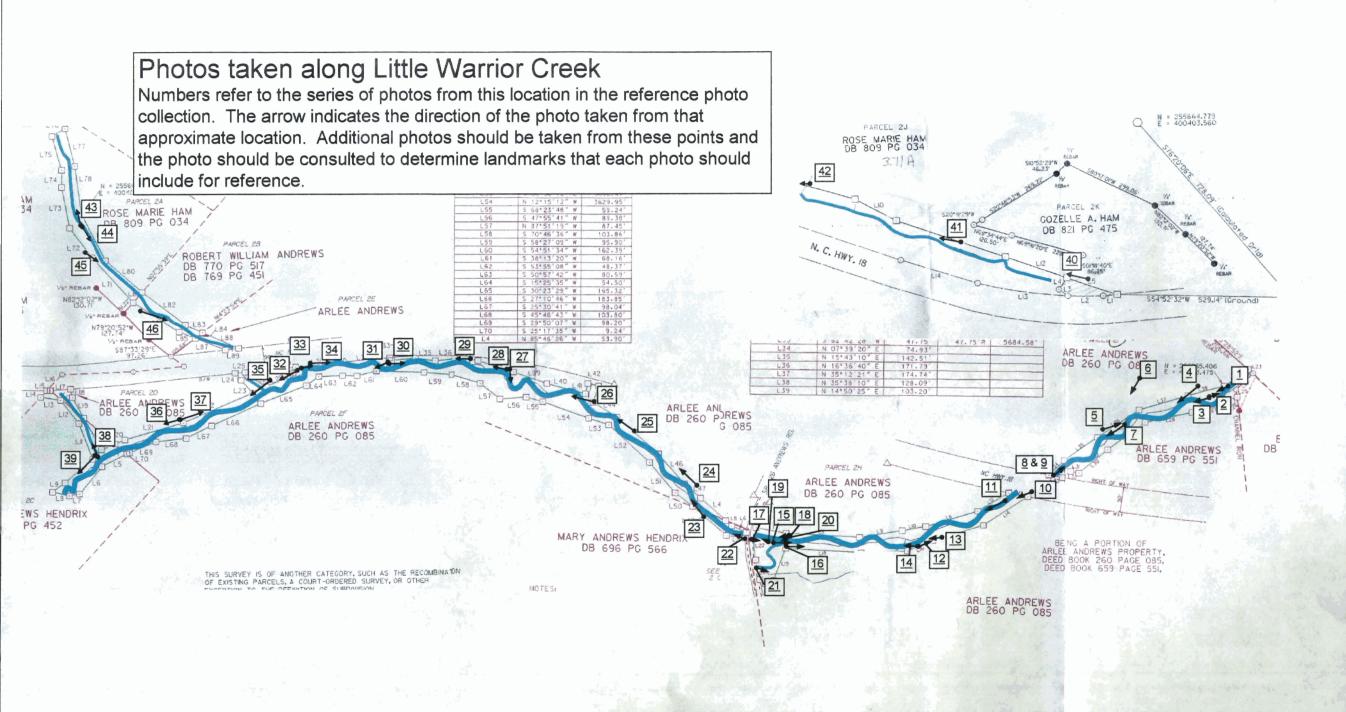
Survey
Project modifications
Reference Photo Locations
Photos of Big Warrior Creek
Pebble Count Data
Cross-section & Longitudinal Profile Locations
Cross-section (Dimension) Data
Longitudinal Profile Data

















DSC00316, 03/1/31

Reach is the lower end of the lower pasture, on Little Warrior Creek. Photos are from the end of the project looking upstream to the lower large willow. This is series number 1 from the LWC reference photos.



US of willow, 01-7-19 thermo & crossing



DSC00320, 03/1/31

Reach is **the** lower end of the lower pasture, on Little Warrior Creek. Photos are taken from just upstream of survey point 2A38 looking upstream. This is series number **4** from the LWC reference photos.



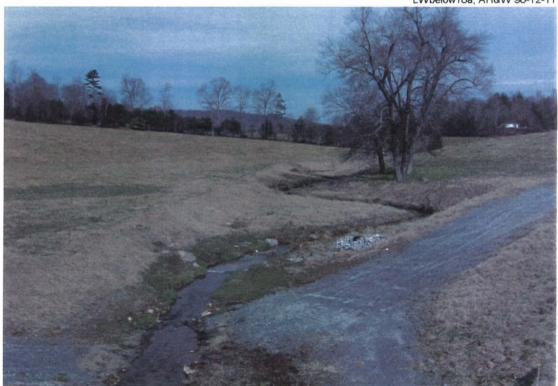


DSC00319, 03/1/31

Reach is at the lower end of lower pasture below Hwy 18, on Big Warrior Creek. Photo is taken from just above the large willow looking upstream. This is series number 3 from the LWC reference photos.







DSC00302, 03/1/31

Reach is the upper end of lower pasture below Hwy 18, on Big Warrior Creek. Photo is taken from on top of the culvert under Hwy. 18 looking downstream. This is series number 8 from the LWC reference photos.



LWabove18a, AH&W 98-12-11



DSC00304, 03/1/31

Reach is above the Hwy 18 culvert, on Big Warrior Creek. Photo is taken from slope below Hwy. 18, looking upstream towards Andrews Road. This is series number 10 from the LWC reference photos.



MVC-0016S, AH&W 98-12-9



DSC00313, 03/1/31

Reach is below the culvert on Andrews Road, on Little Warrior Creek. Photo is taken from the right side of the culvert looking downstream towards Hwy. 18. This is series number 17 from the LWC reference photos.



LW-Rta, AH&W 98-12-11



DSC00314, 03/1/31

Reach is above the culvert on Andrews Road, on Little Warrior Creek. Photo is taken from the right side of the culvert looking upstream towards Hwy. 18. This is series number 22 from the LWC reference photos.





DSC00314, 03/1/31

Reach is in the upper pasture south of Hwy 18 on Little Warrior Creek. Photo is taken from the left side of the channel looking upstream towards upper end of cattle crossing. This is series number 32 from the LWC reference photos.



Lwbypassed culvert, AH&W 98-12-11

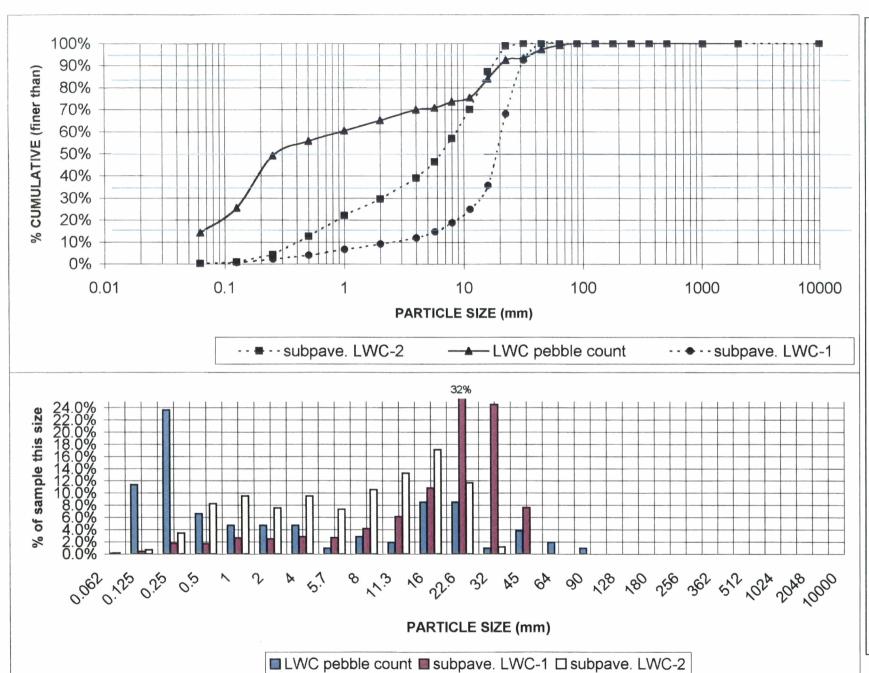


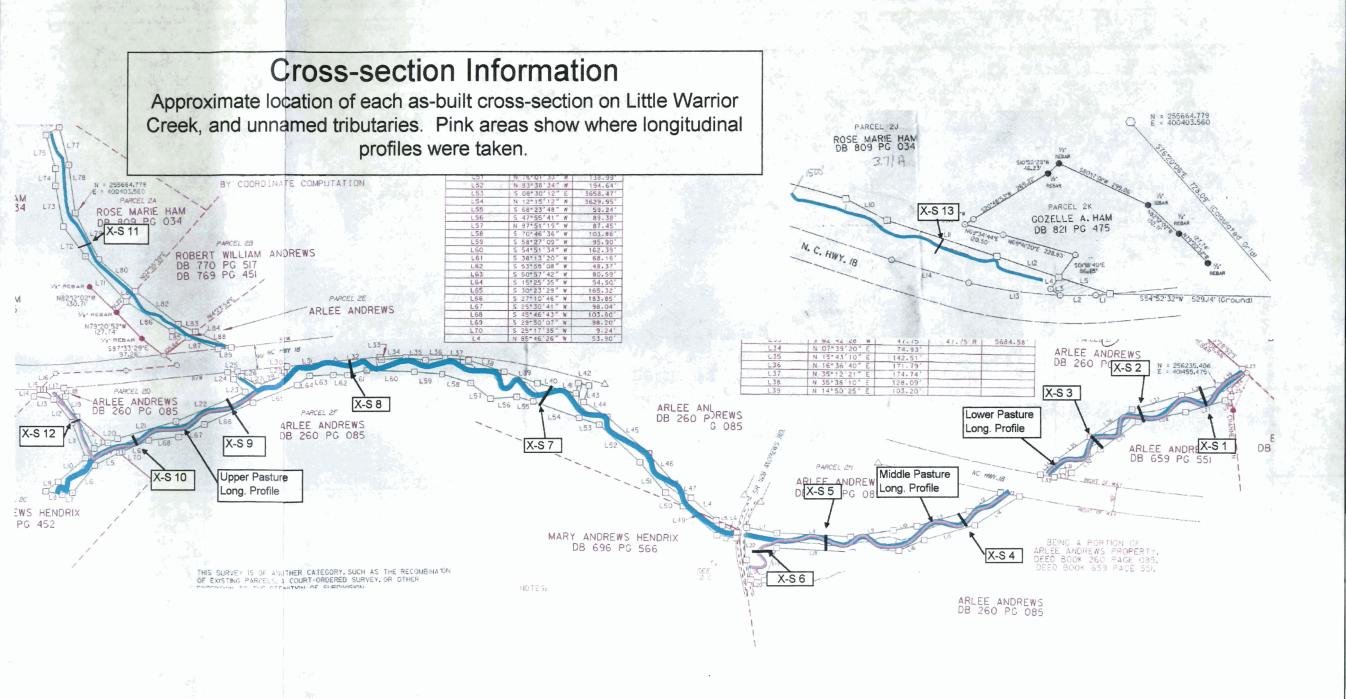
DSC00314, 03/1/31

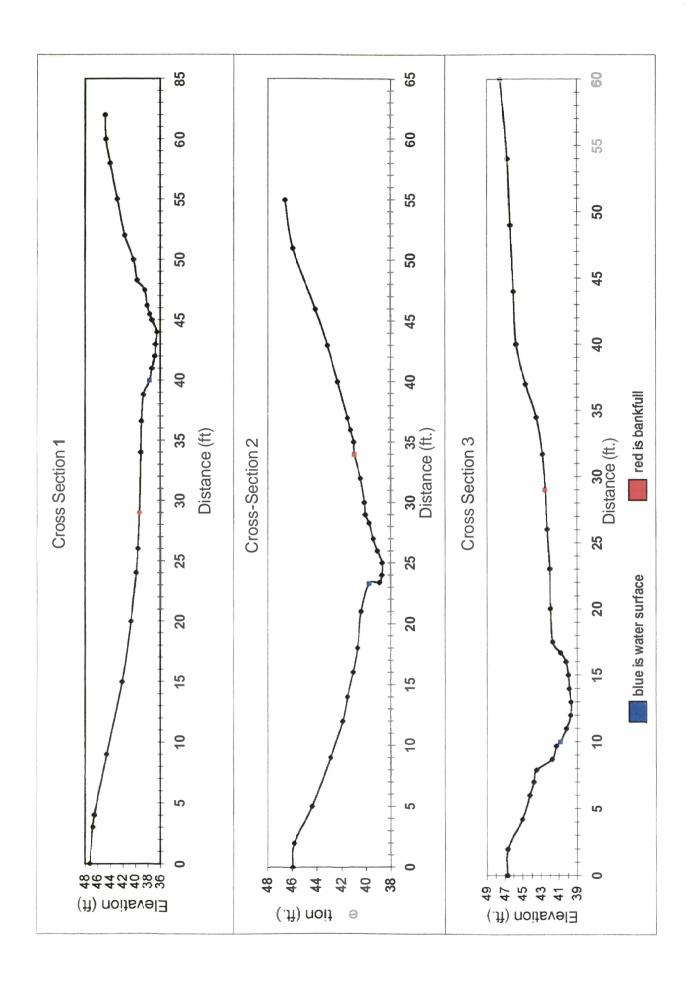
Reach is the upper tributary the crosses Hwy 18 on Little Warrior Creek. Photo is taken from the confluence looking upstream towards the highway. This is series number 38 from the LWC reference photos.

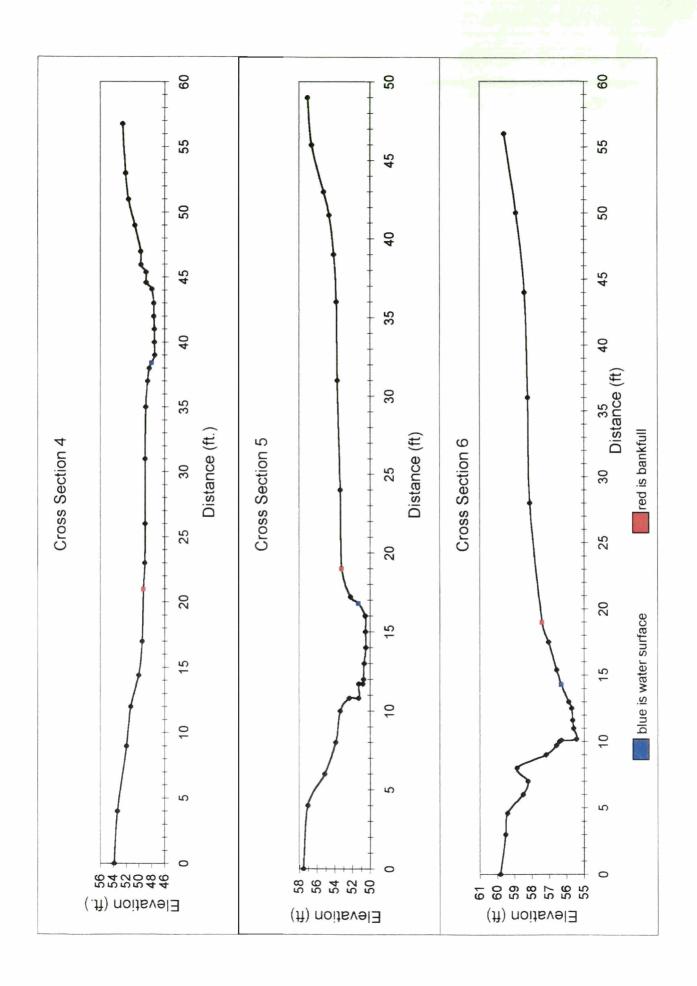
Pebble Count Information from Little Warrior Creek

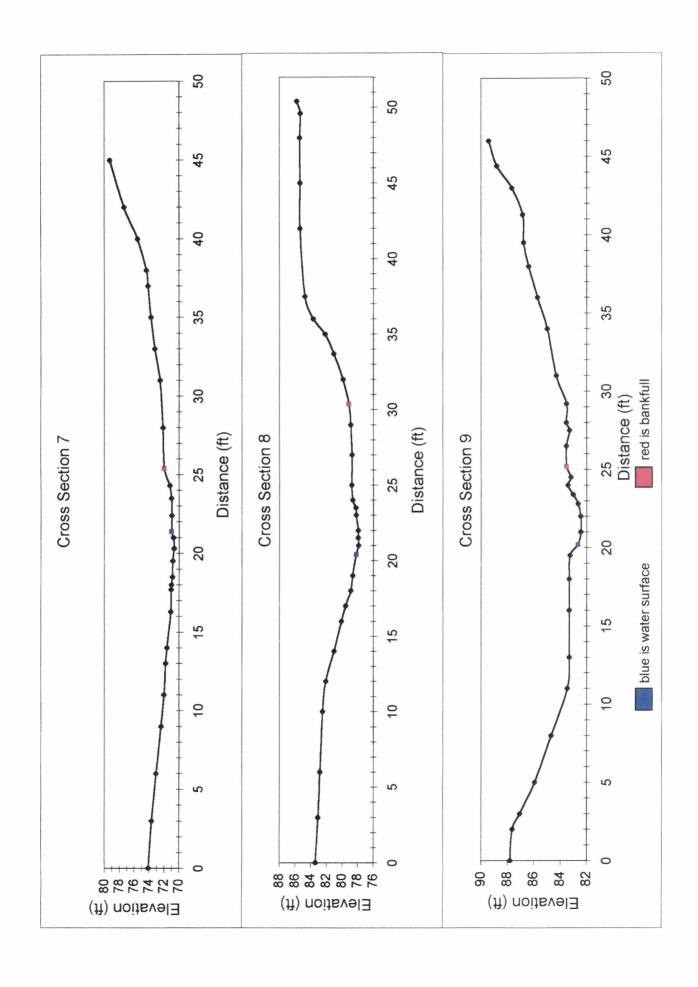
_			_				_		_				_				_	_		_						_		
I		LWC-2	% CUM	%0	1%	4%	13%	22%	30%	36%	46%	21%	%02	%28	%66	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	
PEBBLE COUNT	5/17/01	Reach: subpave.	WILLEM %	%0	1%	3%	8%	9%	8%	%6	7%	11%	13%	17%	12%	1%	%0	%0	%0	%0	%0	%0	%0	%0	%0	%0	%0	
ad l	Date:	Reach:	TOT WT.	4	18	28	508	240	191	240	186	797	332	433	295	30												2535
TN		LWC-1	WCUM	%0	1%	7%	4%	%2	% 6	12%	15%	19%	72%	36%	%89	95%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	100%	
PEBBLE COUNT	12/6/00	Reach: subpave. LWC-1	ITEM %	%0	%0	7%	7%	%8	7%	3%	3%	% *	%9	11%	35%	24%	%8	%0	%0	%0	% 0	%0	%0	%0	%0	%0	%0	
PE	Date:	Reach:	TOT WT.	3	13	54	25	82	77	89	83	129	191	337	1005	762	237						٠					3114
		ble count	% CUM	14%	25%	49%	%95	%09	65%	%02	71%	74%	75%	84%	95%	83%	%26	%66	100%	100%	100%	100%	100%	100%	100%	100%	100%	
	3/17/01	Reach: LWC pebble count	ITEM %	14.2%	11.3%	23.6%	%9:9	4.7%	4.7%	4.7%	%6.0	2.8%	1.9%	8.5%	8.5%	%6.0	3.8%	1.9%	%6.0	%0.0	%0.0	%0.0	%0:0	%0:0	%0.0	%0.0	%0.0	
	Date:	Reach:	# TOT	15	12	25	_	2	5	2	1	3	2	6	6	ļ	4	2	1									106
COUNT			PARTICLE (,																			TOTALS:
PEBBLE C				S/C	တ	4	z	۵	S		ပ	œ	∢	>	ш	7	S		S	0	В	7	В	7	٥	R	10000 BEDROCK	
١				0.062	0.125	0.25	0.5	-	2	4	5.7	8	11.3	16	22.6	32	45	64	06	128	180	256	362	512	1024	2048	10000 E	
			MILLIMETER	< .062	.062125	.12525	.2550	.50 - 1.0	1-2	2-4	4 - 5.7	5.7 - 8	8 - 11.3	11.3 - 16	16 - 22.6	22.6 - 32	32 - 45	45 - 64	64 - 90	90 - 128	128 - 180	180 - 256	256 - 362	362 - 512	512-1024	1024 - 2048		
	Site:	Party:		Silt/Clay	Very Fine	Fine	Medium	Coarse	Very Coarse	Very Fine	Fine	Fine	Medium	Medium	Coarse	Coarse	Very Coarse	Very Coarse	Small	Small	Large	Large	Small	Small	Medium	Lrg-Vry Lrg	Bedrock	

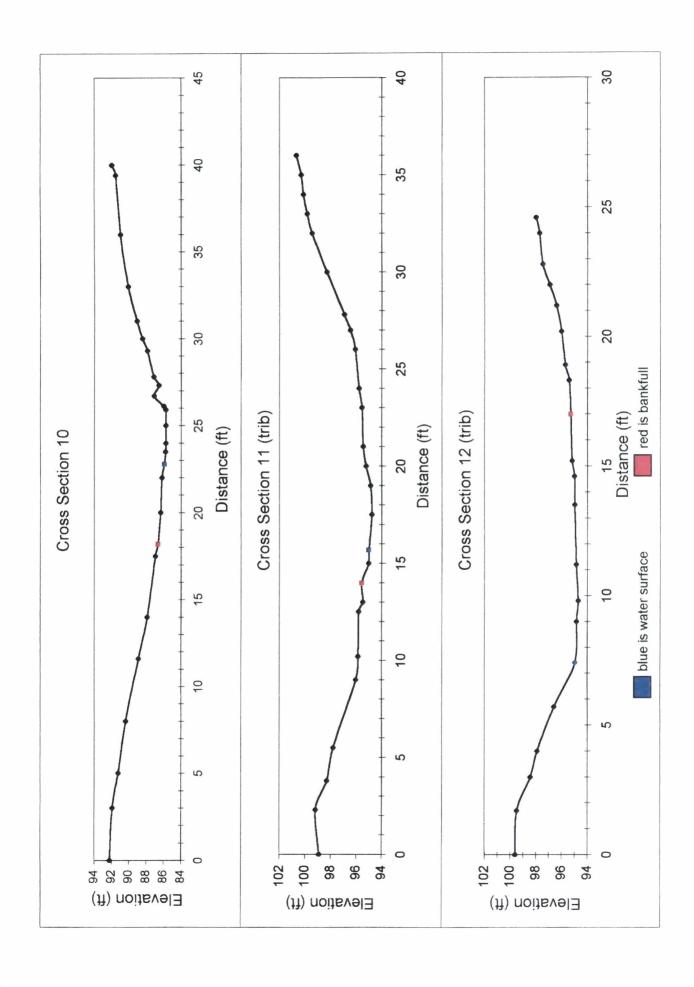


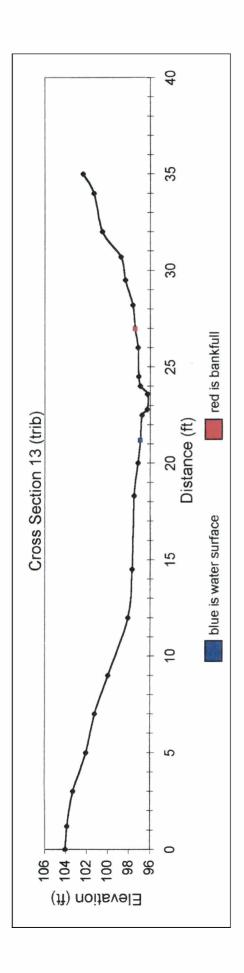




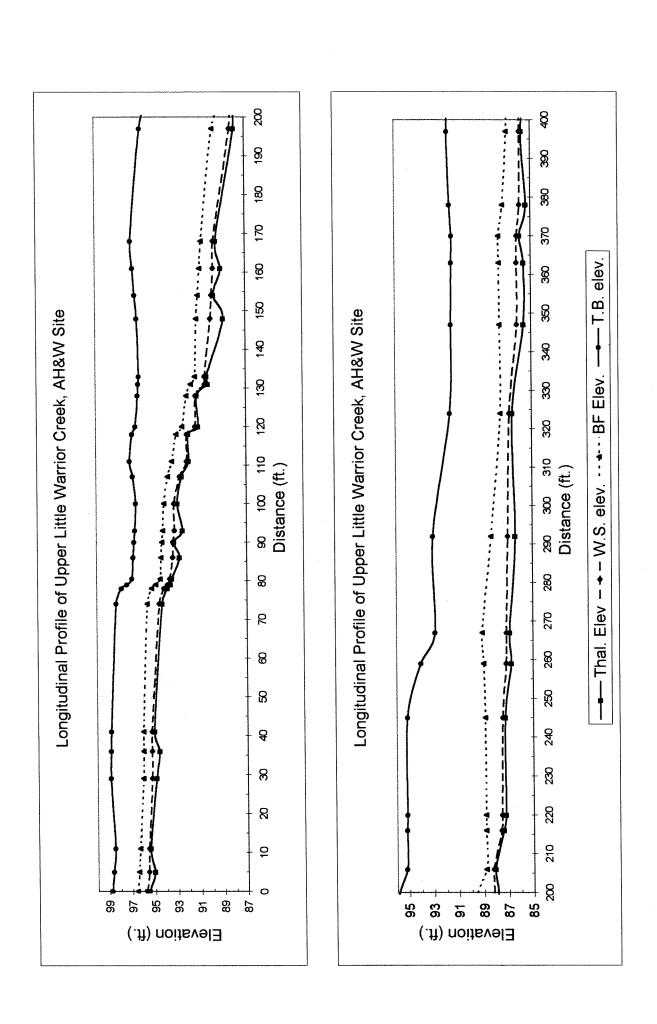


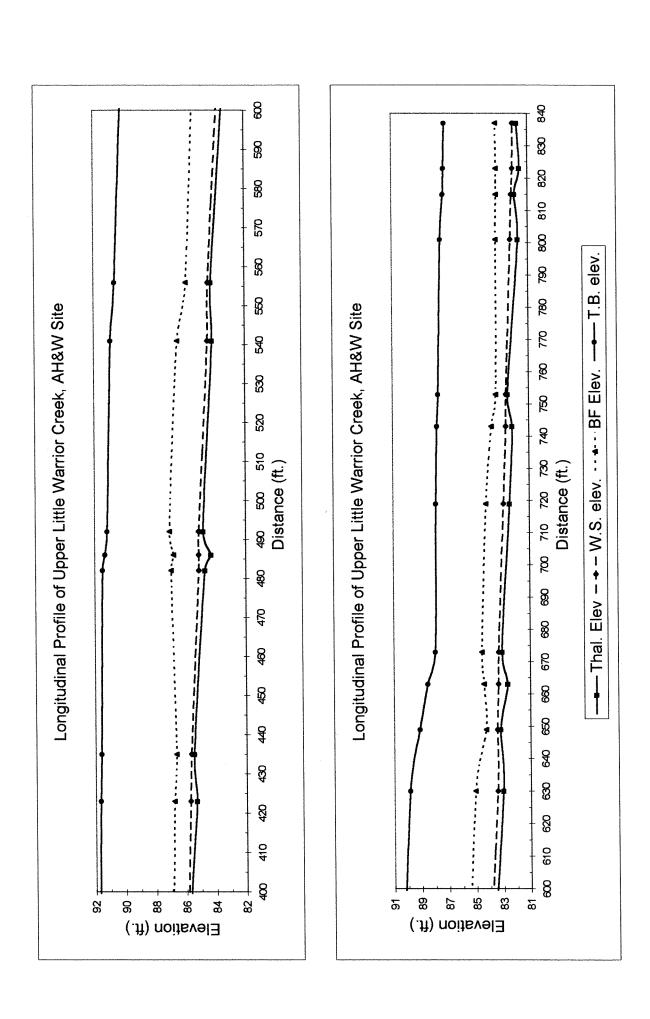






Long	i	tu	di	in	al	F	r	of	fil	le	Ι	n	f)1									t	he	•	U	r	Ţ	e	r	P	a	st	u	16	•	01	n	I	i	tt	le	, 1	W	a	11	ric	01	. (Cr	e	ek		_		 -								
LOUE	KF-W.S.	0.82	0.79	0.78	0.76	1.06	1.08	1.02	0.83	0.94	0.98	0.88	1.01	1.27	0.92	1.13	1 33	0.84	1.22	1.18	1.19	1.06	1.52	0.61	1.26	1.31	04.	7.07	1.85	0.73	1.42	1.43	1.49	1.37	1.65	2 5	1 84	1 88	1.96	2.00	1.47	1.62	0.83	1.8	1.21	1.00	0.75	1.08	1.12	1.24	12.1		1,30				2							
1	Thal	3.23	3.09	3.98	4.23	4.01	3.99	3.79	3.46	3.45	4.13	3.58	4.23	5.09	4.83	5.43	90.0	2002	7 48	6.80	7.60	7.31	8.12	7.08	7.78	7.93	3.5	/7./	0.07	200	5.86	5.83	5.48	6.18	9.00	0.30	, t	100	8.34	6.71	6.37	6.83	5.90	5.86	6.4	5 54	5.12	5.73	5.28	5.58	1000		5.93	1			3.09							
	7:P TB	59	l_	57	1	+		1	+	+	18		-	6	1	=		+	13		36		23	+	+	eg eg	- 6	3	75	3	31			45	+	B	9	B	-	89	-	33	1	8	\dagger	e e	8	22		14			49.8	10:01		ŀ	89							
		2	18		1	7				6		E			2	ľ	7	44	2	_		29		14		1	*		2	1,5			80		28	,	ì	Ţ	49	L	74		14		2	ļ	48		89	14			1 29.2			-	74							
RIFFL	Door L	,	9	12				1	_	2		4	L	7	5	3	,	1		-		24		72	-	25	25		17		22		7.1	19	1.22	-	7	-	2.05	15	1.66	19	1.06	위	1.49	-	0.87	14	1.37	4	ì	О	1 28 12	701		L	0.72 2 2.25 32							
瓷	pool riffle		0.93	1.16	- 1	70.0	$\left \cdot \right $	+	- 5	1.56	1 60	-	-	1.44	1.01	1.38	0.87	1.48	233	7,7	1.84	-	1.9	0.72	+	1.62		2.22	7.7	200	1.97	-	-	1.9	_	1.5	30.0	C7.7	+	2.31	┺	2.05	_	1.74	+	- 54	\$0 C	1.65	1	1.74	1	$\ $		1.87		-	min 1.16 0.							7
next	delo	H	+-	0900	0.0070	0.0340	0.4625	0.3083	0164	0.0225	1.	0357	.0625	0300	1400	0262	0183	02/5	0287	0220	0229	0530	.0933	.0020	.0050	8008	0807	1413	0.0044	0050	0038	.0029	0.0206	3.0087	.0019	.0042	0000	0425	0067	0.0187	+	0389	0411	3.0575	0020	0046	0000	0.0154	0.0075	0.0043	5		Average	El 405-			m m					alley	891108	201100
LHBW site starts on tributary at culvert mouth below Hwy. 18 and sontinues ds to the confluence with the next algoryeanner tree.	elev. s		•		98.805 0	•	.845 0	3825 0	06.92	96.83 0	26.64	96.56	36.81	0 90'76	96.85 0	96.57 0	96.36	305	20.60	56.57	96.73	98.89	96.05 0	35.21 0	95.19 0	35.17	35.15	94.02	92.89	24 57	91.45	91.39	91.37 -(91.54 -(91.7	91.65	91.6	91.46	91.49			89.85	89.11	88.54	87.96	87.87		87.46	11	87.18	7	H	- A	<u>}</u>			Range:					difference from top to bottom of the valley	Sinuositv= 0.891108	DSILY-
onfluence	1.8	6.36 9		6.3	\perp	6.3/	97	1	8.22			8.58	٠.	8.08		_	8.78	6	_L	1	+	8.25	L	5.29		1	5.35		7.81		L		9.13		8.8		8.9	+	25.0		9,91		5.08		6.23	+	a 50	L	6.95			H	-	0.0014	5	}	<u>ac</u>					o to bottor	S	2
s to the o	Top ba	9	\downarrow	L	Ш				1				L	L			8		١		\perp	L	L		-		1	4	`	ľ			L				1	1	ľ	1	L					1							_					igt	ĺ			e from top	α	o o
ntinues d	slope		0.0250	0.0040	0.0040	0.0755	0.0755	0.0755	0.0175	0.0175	0.01/0	0.0173	0.0710	0.0760	0.1020	0.0760	0.0740	0.0740	0.0290	0.0290	0.0290	0.1970	0.1970	0.0000	-0.0020	-0.0020	-0.0210	-0.0210	0.1500	0.1020	0.000	-0.0040	0.0680	0.0680	0.0260	0.0260	-0.0580	0.0320	0.0560	0 1180	0.1610	0.1610	-0.0280	-0.0280	0.0680	0.0900				-0.0020			-	0.0064	2			ank to la				differenc	0.0148	5
18 and co	F Elev.	96.59	96,465	96.02	98	95.98	95.225	34.8475	94.47	34.3825	34.75	94.12	93.765	93.41	93.03	92.52	92.14	91.77	91.4	91.200	90 965	90.82	89.835	88.85	88.85	88.86	88.87	88.975	89.08	88.33	87.56	87.58	87.6	87.26	86.92	88.79	86.86	86.94	86.78	86.47	85.88	85.075	84.27	84.41	84.55	84.21	83.76	83.375	83.33	83.34	83.35		a700 0	0.0078	73776			top of b		800	87.12	11.66	E GCC	Slope -
ow Hwy.	3F BF	8.55	00		1	9.16		_	10.67	+	+	11 02	٠.	11.73			13		13./4	+	t	14.32	4-	11.65			11.63		11.42	-	-	\dagger	12.9	-	13.58	-	13.84	+	1,	-	14.62	+	9.82		9.64	+	10.7	10.01	10.86	1	10.84		- 0000	0.0029	0.0032		=TOTAL	Valley slope from head of 1st top of bank to last		nce II	arık - pank≕ _		Valley Stone	Valley
nouth be	8	9	9 5	V 2	Q.	60 5	2 8	37	73	9	2;	4 8	2 5	2	8	75	8	99	3 5	6 5	g	18	2 82	20	90	32	23	55	49	g s	200	57	75	=	58	28	17	8	8 8	R	2 6	98	84	10	93	87	33	64	37	4	186	H	Ш	0.0167			837 =TC	om hea		dista	last top of bank =			
culvert	dols	7 0.0380		0.00	4 0.002	3 0.020	4 0.310	3 0.126	4 0.04	0.0050	0.04	200	0.00	000	1 0.36	0.00	3 0.2600			3 0.016/			1 0.0078	4 0.08	9 0.01	5 0.003	7 0.0229	5 0.00	3	000	20.0	000	1 0.02	00.0					0.0000					0.0010			7 0.00	3 0 0064	٠.		-0.098	\perp		-	18		8	slope fr		1	ast is			
ibutary at re tree.	W.S. elev	95.7	95.5	95.2	95.2	95.2	94.14	93.8	93.6	93.3	93.3	93.2	7 60	92.1	92.1	91.3	91.33	90.5	1	1	1		88.3			87.5	87.4	87.1	87.1	86.9	80.78			85.89									1	83.35			82	82.5	82.21	82	82.08		1 11	-0.0050)	П	67%	Valley						
AH&W site. e starts on tributing sycamore	W.S.	9.37	9.56	80.8	6.6	9.91	17	11.31	11.5	11.76	11.78	11.91	10 38	13	13.03	13.75	13.81	14.59	14.58	15.11	15.21	15.38	12.19	12.26	12.91	12.85	13.03	13.35	13.37	13.53	13.77	14.35	14.39	14.61	14.63	14.78	14.85	15.4	15.4	10.4	16.05	10.74	10.75	10.84	10.85	11.28	11.49	11.52	11.98	12.09	12.11		2700 0	0.0073	0.0416	29.2	558					valley		
er by Green	slope	10	90.0	3 2	60	20;	0.27	60	12	-0.12	38	70 80	9 4	2 2	4	.02	0.33	50	9	-0.14	3 5	3 8	2000	70.	-04	00.	70.	7.02	8	5 6	40.0	3 5	0.07	7.02	0.02	0.01	25	9	90.0	5 8	000	150	2	-0.04	10.	10	898	202	200	9	0.10	\vdash	- 0	0.0043	slope=	length	length	1000	1			ence from top to bottom of the valley		
Information Long-pr tributar	lev sic		- 1	1	1 1	1	93.86		1		1	- 1	1	1	1			- 1	ļ	-1	1	1	87 93	L	Ш					_		L	L	95,36				_1		1	24.70			82.67 -(Ш	_1	2.22	73 5	96	81.6	1.78	+	H.	214	Avg. Riffle slope=	vg. Riffle	otal Riffle	of last pool				p to botte		
for: As-built description:	Thal. E		-			1			П		-	-			l			- 1		-		1									1	1		1				1	1	1	1						١					-	Ш	- 1	L			bottom				e from to	;	34
Sheet for Profile de	Tha!	9.56	O	10.25	10.56	10.1	11.2	11.5	11.6	12.3	11.8	12.6	12.7	13.1	13.1	Ť	13.8	14.8	14.7	18.2	15.3	15.0	12.5	12.3	13.0	13.2	13.2	13.7	13.6	14.1	13.9	4 0	14.6	15.1	14.	15.2	- {		- 1	- 1	- 1	1	1	1	1 3	- 1	- 1	•	1	12.59	- 1			0.0050			33%	e 5				žЩе	ć	0.0164
file Data	10		9	8	5	33	4 -	1.5	5.5	4	8	+	1	F	C	8	9	2	15	9 1	1	200	20	5	4	52	14	63	25	32	23	2 1	. α	19	28	12	47	4	9	9	2 5	19	4	10	46	24	9	48	ŧα	14	-837			0.0000	0.0164	12.1	th 279	d of 1st		837	95.77 82.08	13.69	1	edole =
Longitudnal Profile Data	enoth Tot.	+-	2	11	36	# !	787	79	80.5	98	8	8	100	177	118	120	128	131	133	148	154	0 00	107	206	216	220	245	259	267	292	324	363	370	378	397	423	435	482	486	492	247	300	648	663	673	719	743	753	212	823	837	\dagger		0000	.003z	ength	length	om hea		ıce ≍	= dot pottom =	I	4	Water Surface Slope =
Longitu	-			1							1			1					-	-											1	1									1										1	+			opes= 0.0032 Avg. slope=	Wd. Pool	otal Pool	slope fr		distance	8	!	0,117,	Nater 5
	L		Ц	105	105.	105		L	L	Ш	_	1	1	1	L	105	105	Ш	- 1	- 1	- 1	1	- 1	12	9	9	2	٩	5	9	219	1	15	+	╀	Н	\vdash	Н	+	=	2 5	200	96	8	20	ģ	ŏ	ŏ	» S	94.19	6	-	Ш	1	Pool slopes	1		Water surface slope from head of 1st riff					-	
	Feature	culvert lip	HoP	Ton	Deep	HoR	riffe Diffe	riffe	riffe	Hop	TOR	유	권	5 00	1 2 E	윤	Top of xv	모	Top of xv	Hop	Top of xv	100	HOH	Hon	riffe	a of	HoH	Hop	HoR	ē	면임	Hoh	ELOD D	1 2 2	79°E	4 6 6	HoR	HoP	thalwag	완	d c	2001	2 2	모	HoR	riffle	HoP	유	100	HoP	HoR							Waters		-			-	

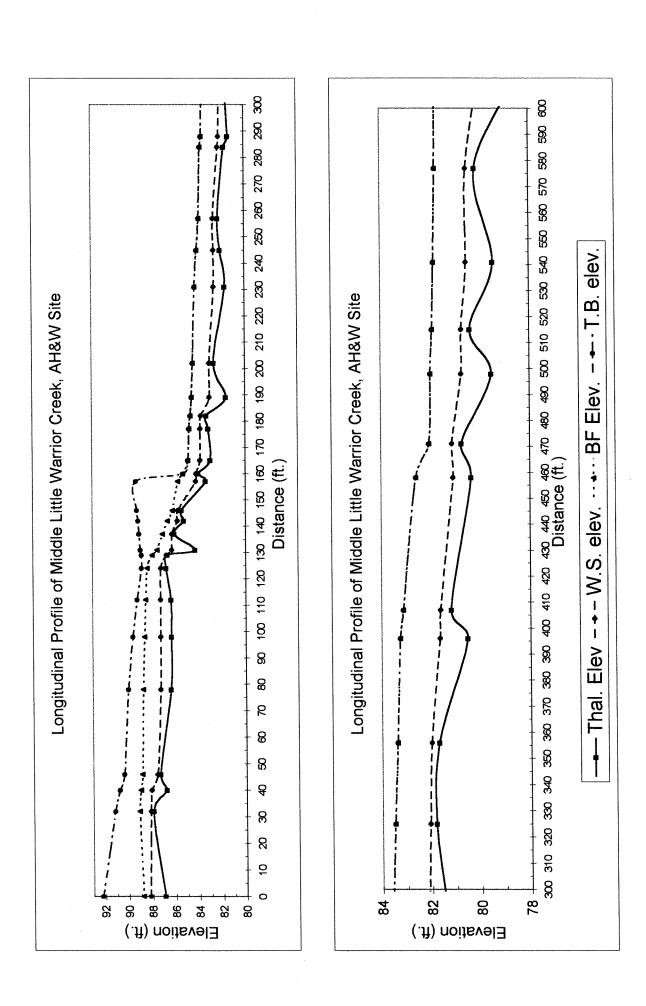


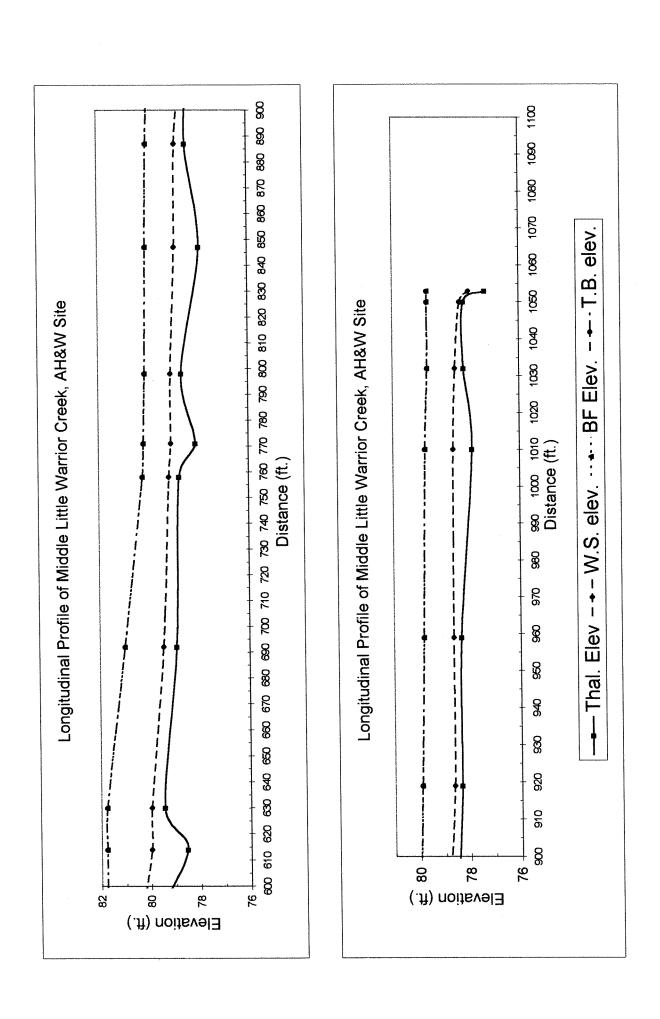


Longitudinal Profile Information for the Middle Pasture on Little Warrior Creek

1	_	188.0			1.47	1.37	1 160	8	1.24	181	7.84	7.44	1.52	200	3 4	gg	152	9	1.63	1.42	1.21	1.51	1.46	1.42	음 등 등	3 2	12	0.93	1.25	1.19	1.32	1.25	8 8	38	1.06	1.10	1.04	1.16	4 00	1 10	1.12	=	1.29	1.65	T		1.24			0.44	0		
al Bkf-W.S	L						1						1	-	1	1					. 09	04							1	Ì				2.08			47	15	200	20	98	45			+	-	2.41				_		
TB-Thal	5	6	_		\sqcup	m c	10	2	4	2	3	Ċ.	Ċ.	1	<u> </u>	+	-10	- -	_	-		4	- 12		- 0	7	1	ļ	-	L	Н		4	7 2	-	Ц	4	4	1		1	L	-	2	1		5			1.29			
RP	40	8	38	32	83	\perp		-	=		15		8	-	24	7	4	62	53		27	112	4	11	8	70	4	27	₹	26	73	37	15/	-	ŀ	76	49	163	23	+	43	21			+		43.7 58.			ω ξ	-		
pool-L riffle-L		5	9		46	+	+	ļ	=		15		8	- -	17	+	13	Ĺ	26			41	1	+	;		2	L	17		36		16	+	-	27		40	+	+	22	L	-	က	+	\vdash	21.2 43			5	\dashv		
_		1,2	ŀ	1.55		+	63	3	-	-	-			+	+	1 22	3	162			9.1		-	1.67	+	20	CS.	32	-	1.54		.62		75.7	╀		.47	-	26	$\frac{1}{1}$	+	1.45	_		-	-	1.60 2			1.2			
pool riffe	85	+	2.2	1	38	\dashv	+	+	3.19		.38		2.35	-	98.	+	2 94		2.56		Ì	2.04	1	+	- 22	7/7	2 24	-	2.47	1	2.41		3.23	1	+	2.07	ŀ	2.15		+	1.86	┸	<u> </u>	2.3	+		2.32			1.38			
alone	0338	0481	0642	0120	.0192	0275	0.0321	0.000	+	+-	0.0231	-	-	0880	0082	0700	-	+-	+-	0.0161	Н	\vdash	0033	0,0040	-	-+-	0.0100	+	+-	+-	Н	\vdash	-+	0.0123	0.0042	1	Н	7	0.0030	00024	0.004	0.000.0	00000	15.9260			Average=			mim	max		
Vala	170 00	1		1	1 1	ŧ	89.24 U	1	1					- 1			4		ŧ	1	1 1	1 1	1	- 1	ŧ		83.13		1	1		1 1	- 1	81.70	1		1	- 1	- 1	- 1)	1		1 1	-		¥			Range:			
nk TB	L	1 93		-		+	100		+	-	-				3.5	+	+	3.4		_	4.73		_	-	+	\perp	68.9	7.55		_		7.83	-	8	60.6				9.87	+	+	11.1			+	-	331	m		L	_		
Tob ba		-						Í													4					(٥	7				7			6				6								-0.0031					정	
clone	0100	0.015	0.020	0.004	0.006	600.0	0.010	0.000	0.220	0.088	0.110	0.040	0.147	0.088	0.00	0.020	C10.0	2000	0.014	0.016	0.005	0.031	0.003	0.004	0.003	0.011	0.010	0003	0000	0.003	0.002	0.000	0.001	0.012	0.004	0.002	0.001	0.001	0.003	0.002	0.00	0000	0.000	15.926			0.0027					ank to la	
FELOV	20 70	80.73	88 99	88.87	88.75	88.62	88.50	00.00 07.00	87.5	87.06	86.62	86.18	85.74	85.3	84.86	84.76	84.55	84 45	84.26	84.06	83.87	83.75	83.62	83.50	83.38	83.25	83.13	82.08	81.99	81.92	81.85	81.78	81.77	81./6	80.24	80.19	80.13	80.08	80.02	78.87	79.73	79.63	79.63	79.63			0.0111					Valley slope from head of 1st top of bank to last	
BF BF	Ę	3 98	3	-			12.1	4.71		-	-	-			8.23	\dagger	1	8 64			9.22				+	- 6	98.8	11 03	20:-	$\frac{1}{1}$	-	11.31		11.33	12.85	-			13.07	+	T	13.46			1	$\frac{1}{1}$	-0.0011		0.0068	=TOTAL		ad of 1st	
F	╀	900	867	100	0.000	011	0.0014	200	347	940	0.0100	382	0.0033	700	042	8 5	0.1043	145	110	3013	156	200	022	970	087	027	0.0104	144	900	770	000	0.0151	900	0.0084	690	000	035	0.0010	075	0000	0.0000	8	0.1200		+	+	-0.0015 -(1 11	- 1	1058 = 1		rom hea	
200													1 1																	i i	1	1 1	1	- 1	1	1	1	1 1	- 1	1	- 1	1	1	1 1	+				Avg. Pool slope=	%29		slope f	
MV S. off		8	88	87.5	87.	87.2	87.2	70	8 8	98	85	85.	84.	84.	83.	83.	83.	88	8	82.6	82.	82.	82.	82.		8	9	ō	8	8	80			79.96						-							0.0042		A	79		Valley	
notes at DC	00 4	4.36	504	5.53	5.82		0.0	79.0	683	8.84	7.31	7.35	8.87	8.88	9.23	000	9.33	\$ 50.00	10.46		10.43	10.85			11.09	11.44	11.47	11 06	12.35	12.36	12.56		13.12	13.13	13.94	14		14.17	14.21	14.45	14.40	14.57	14.75	15,11			II.			929		lood	
se orner	adous	57.62	5 6	600	800	0.00	0.03	0.02	200	0.16	-0.05	0.19	-0.21	0.20	-0.01	-0.04	0.24	00.00	200	0.02	0.02	0.08	-0.01	0.00	0.03	90.0-	0.02	35.5	50.0	0.00	-0.05	0.04	90.0-	0.01	0.00	-0.02	0.01	-0.01	00.0	0.00	20.0	000	0.28	15.47			0.0100	0.0010	le slope=	iffe length		of last	
70 11 104	100	- 1	1	1	ł	1 1	86.35	- 1	- 1	- 1		1	1	1 1	1	- 1	- 1			ŧ	1	1 :	1 1	1 1		ŧ		- (- 1		1	1 1	, ,	79.44		1	1	1 1		t	- 1			1		1	0.0017	0.0000	Avg. Riff	Total Riff		to botton	
ľ	-1	0.0 0.0	0.10	577	6.72	6.77	6.74	45 6	6.43 8 78	7 03	7.85	7.65	9.7	90.6	10.09	9.95	9.77	04.1	1130	1101	10.82	11.38	11.71	11.26	11.4	12.56	11.91	14.73	13.57	12.71	13.65	12.93	14.55	13.65	14.17	14.97	14.43	15.16	14.63	14.74	14.70	14.91	14.91	15.76		+	0.000.0	0.0006	1	38%		1st riffle	
	IOL DISE	37	0 4	33.0	8	14	12	n	7 4	מע	7	-	က	5	12	2	7	2 6	14	12	27	4	37	31	40	11	51	51.0	17	28	38	37	16	62	200	27	49	40	32	Q 7	5 6	18) m	2			11	6	0.0097	402		Water surface slope from head of 1st riffle to botton	
L	- Infilia	0 0	700	46	78	98	112	124	128	137	142	146	157	160	165	177	182	882	234	245	257	284	288	325	356	396	407	428	471	515	541	277	614	830	758	771	798	847	887	919	808	1032	1050	1053	1058	+	3.0016					ope fror	
F		93.09	80.00	93.00	93.09	93.09	93.09	83.8	93.09	80.08	93.09	93.09	93.09	93.09	93.09	93.09	83.09	83.08	93.00	93.09	93.09	93.09	93.09	93.09	93.09	93.09	93.09	83.08	83.03	93.09	93.09	93.09	93.09	93.09	93.08	93.09	93.09	93.09	93.09	93.09	83.08	93.09	60 66	93.09	93.09	1) =sedols		Avg.	Total Pool length		rface s	
	Leature	+	1	\top	음	\vdash	1	1	lop of xv	-	-	-	HoP-dep			ge		deb	200	Т	고 모	T		П	thalwag			deb-	707 107 107	_	aep		HoP-dep	-	thalwag	T	-	HoP-dep	_		Thalwag	_	3	Т	culvert inv		Pool sl			Tc		Water su	

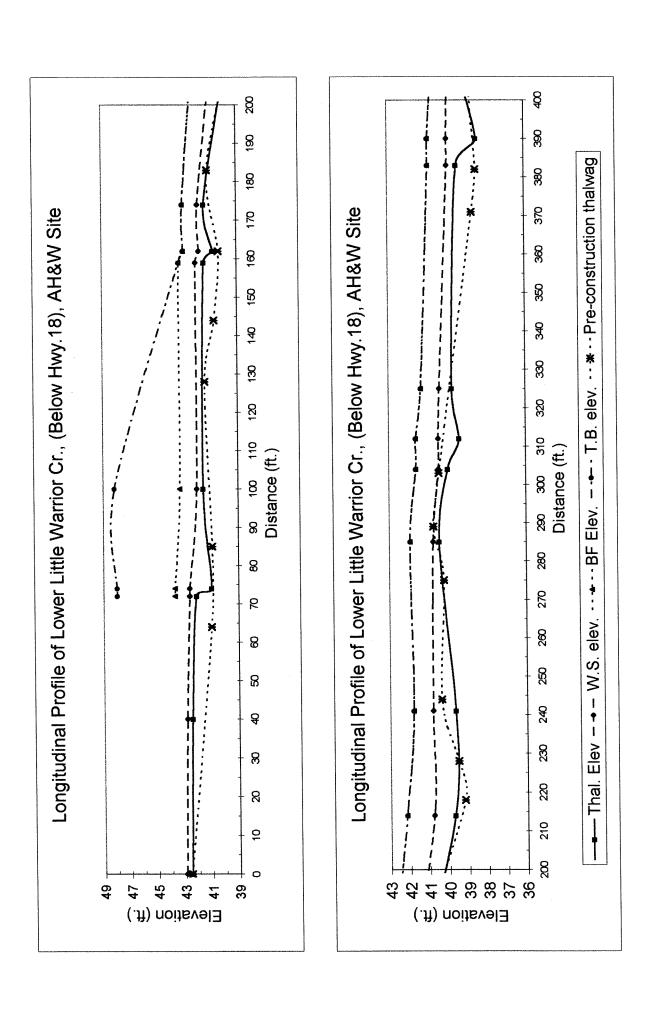
Valley slope from head of 1st top of bank to last	distance = 1058 1st top of bank = 92.24 last top of bank = 79.63 12.61 difference from top to bottom of the valley	Valley Slope = 0.0119 Sinuosity= 1.232649
urface slope from head of 1st riffle to bottom of last pool	distance = 1058 top = 88.21 bottom = 77.98 10.23 difference from top to bottom of the valley	Water Surface Slope = 0.0097

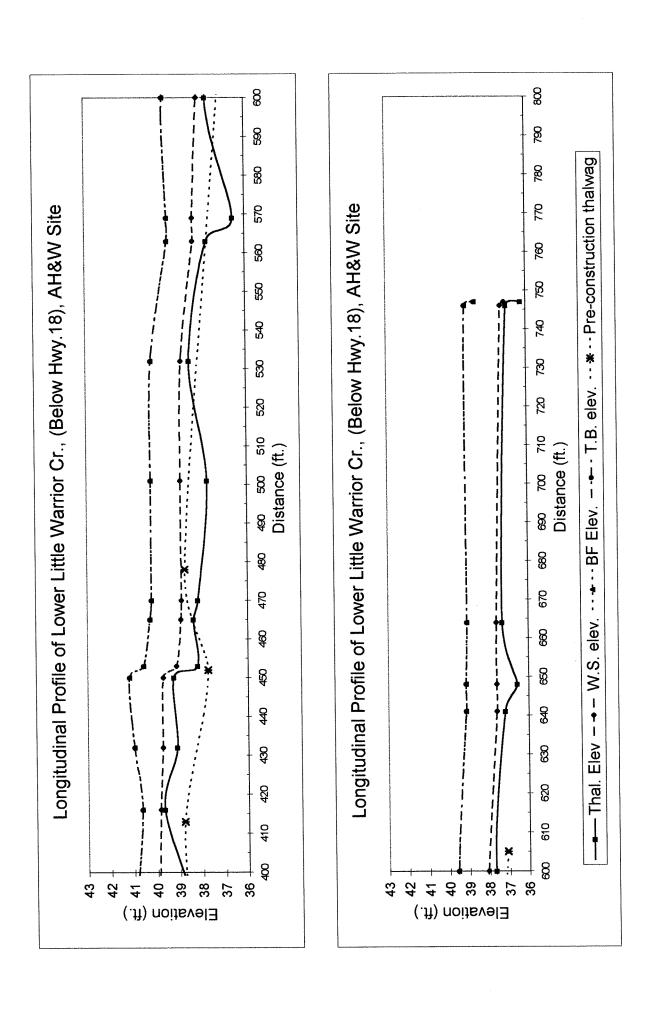




Longitudinal Profile Information for the Lower Pasture, Little Warior Creek

	Longit	udinal Pro	file Data S	heet for:	As-built infi	Longitudinal Profile Data Sheet for: As-built information on AH&W [Profile description: Long-profile starts a	AH&W site.	How Hwy.18	site. at below Hwy.18 @ starting at box culvert mouth, centered on	at box culve	ert mouth,	centered o	Ē								
																740	OCC HER	TOOG:			
Coopile		l aposth	Tot Diet	Tha	That Fley	slone WS	Ĭ.	W.S. elev	slope	BF B	BF Elev.	Slope	Top bank T	.B. elev.	d edols	pool riffle	e	_ -	R:P TB		Bkf-W.S.
Color	50 45	- Carigina	101. 101.	┸	A2 5A		6	L	0.0028	r	52.15	T	4.16	47.99	0.000.0	9,	9.61	74	100	5.45	9.2
halwad-oc	52.15		32		42.45	0.01	9.31	1	0.0069		52.15	0.264	4.16		0.000.0	H				5.54	9.31
-vane	52.15	72	2	7		0.56	9.53		0.000.0	8.46		0.000	4.16	- 1	-+	- 6	-		$\frac{1}{1}$	5.87	1.07
-IOP&deep	52.15		26		41	-0.02	9.53		0.0223	8.46	┙	0.016	4.16		_	2.69	97	60	1/4	6.33	20.
HOR	52.15		59	10.57	1	0.00	10.11	L	0.0000	8.87		0.000	3.99	48.16	0.082/	\dagger	1	70	2	1.85	1 24
thatwag	52.15		8	┙		0.22	10.11		0.0833	8.87	43.40	7000			0.100	20	12	Ţ		2.2	1.17
HOP&deep	52.15		12			-0.05	10.30	41.79	-0.0083	9.6		20.02		42 90	0.005	L	1.58	40	E	1.58	-
HOR	52.15		40	⊥	41.41	┸	10.20	_L	0.0273	0 00	L	0.020			t	2 45	1	L	┺.	2.45	1.37
HOP	52.15		2/	\perp			11.33		0.0004	10.36	1	5003	1	1.	1.	-	: T			2.14	0.98
Deep pool	52.13		44	14.0	39.00	1	11 30	4	0.00	10.22	L	0.017		41.93	0.0168	F	48	27	8	1.48	1.17
10x	52.15		200	L		0.02	11,53	_	0000	10.54	41 61	0000		41.61	0.000	-				1.62	1.14
Thamag	52.15	342	430	12.10	30.30		11.00	_	0.0054	10.54	1	0.022		╄-	+-	2,22	13	3		2.22	1.14
HOP&deep	50.15		58	┸			11.75	1	0.0079	10.82	L.	0.007		┺	┼	匚	.58	58	91	1.58	0.93
HOR HOD	52.13		200		1	L	12.21	1	0.0000	11.22	40.93	0.000		40.93	0.000.0	1.47	33	3		1.47	66.0
Deen nool	57 15		26	1	38.44	-0.05	12.21	39.94	0.0035	11.22	L	0.011			0.0108	H				2.49	0.99
200	57 15		16	L		1_	12.3	1	0.0062	11.5	L	-0.021			-0.0206	-	0.97	16	37	0.97	0.8
HOP	52 15		18			<u> </u>	12.4	1	0.0017	11.17		-0.012		40.98	-0.0117	1.87	2	=		1.87	1.23
x-vane	52.15	450	3	1_		0.35	12.43	L	0.1967	10.96		0.207			0.2067				\perp	1.93	1.47
Hoalide	52.15		12	1	38.21		13.02	l	0.0175	11.58	40.57	0.025		40.57	0.0250	1	_	12	62	2.36	1.44
HOP	52.15	465	5	<u> </u>		l	13.23	L	0.0060	11.88		0.014		1	0.0140	1.9	⁶			1.9	1.35
thalwad	52.15		31	13.97			13.26	ш	-0.0006	11.95	40.2	0.000		40.2	0.000	+	1			2.02	1.31
Deep pool	52.15		31	_			13.24		0.0019	11.95	40.2	0.001			0.0013		7		- 8	2.40	25.
HOR	52.15		31	Ш	38.49	0.03	13.3		0.0181	11.99	40.16	0.024	1	40.16	0.0239	1,77	1.67	31	89	1.0/	5.5
HOP	52.15		9	_			13.86	L	0.000	12.73	┙	0.000		- 1	0.0000	1	9		+	0000	1 2 5
Deep pool	52.15	Ì	31	_	"		13.86	_1	0.0068	12.73		0.000	+	39.42	2000.0-	-	4 00	**	3	1 88	
HOR	52.15		4	14.45		\perp	14.07	_1	0.0117	12.57		0.011	+	39.30	2000	- 1	00.	1	5	98	2 2
HOP	52.15		7	_			14.55	37.6	0.0000	13.01	39.14	0.000		30.14	00000	<u> </u>	1	2		2.56	154
Deep pool	52.15		16	_	36.58	0.00	14.55	37.0	0.0000	13.01	L	0.00		30.08	0000	-	11	83	84	17.1	1.48
JOK E	52.15		78	丄			14.33	- 1	0.0039	13.07	L	780		30.08	0.2800	2 00	<u> </u>	3	L	2.09	18
x-vane HOP	52.15	740		15.10	36.25	0.74	15.06	37.09	0.1900	13.55		i0/AlG#		38.6		+				2.35	1.51
	02.13			2.5							J				Average≖	2.06	2.47 30.40	10 44.40	74.80	2.63	1.76
Pool	slones=	Pool slopes= 0.023	-0.0083	-0.0004	0.0054	0.0000	0.0000	0.0017	0.0060	0.000.0	0.000.0			i	<u> </u>	l]				
	¥	a. slope=	0.0078		L	Avg. Riffle slope=	0.0103	Avg. Po	Avg. Pool slope=	0.0027											
	Avg. Pt	Avg. Pool length	30.4		Avg. F	Avg. Riffle length	44.4				***************************************						-	,	-	100	0
	Total Po	Total Pool length	304	41%	Total	Riffle length	444	29%	747 = 7	=TOTAL				Range:	Ē	1.47 0.	0.97	27.5	٠/٠ ١٠/٠	0.97	8,0
													J		шахі	2.09 9		20	\dashv	-	9.5
Water surface slone from head of 1st riffle to bottom of last pool	acle elor	e from h	and of 1s	t riffle to	o mottom o	Flast pool		/allev slop	Valley slope from head of 1st top of bank to last	d of 1st tc	of bank	to last				Г					
200	200						<u> </u>														
	ĕ	distance =	747						dist	distance =	747										
		top ==	42.95						1st top of bank =	pank⊩	47.99										
		pottom =	37.09	differen	ce from top	37.09 5.86 difference from top to bottom of the vall	the valley		last top of bank=	i bank≕ 	38.6 9.39 di	ifference from	difference from top to bottom of the valley	ottom of the	e valley						
										:	7		•		0						
	Wate	Water Surface	Slope =	0.0078	~					Valley	Valley Slope =	0.0126		Sinuosity= 1.602389	1.602389	٦					

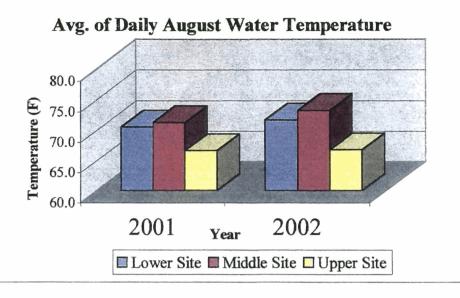


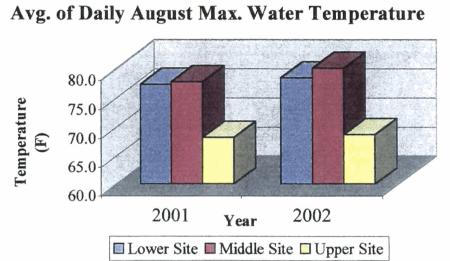


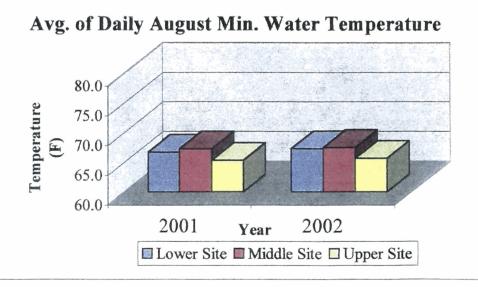
Water Temperature Data for Big and Little Warrior Creeks 2001 and 2002

Locations of Onset Thermometers Big Warrior Creek Little Warrior Creek

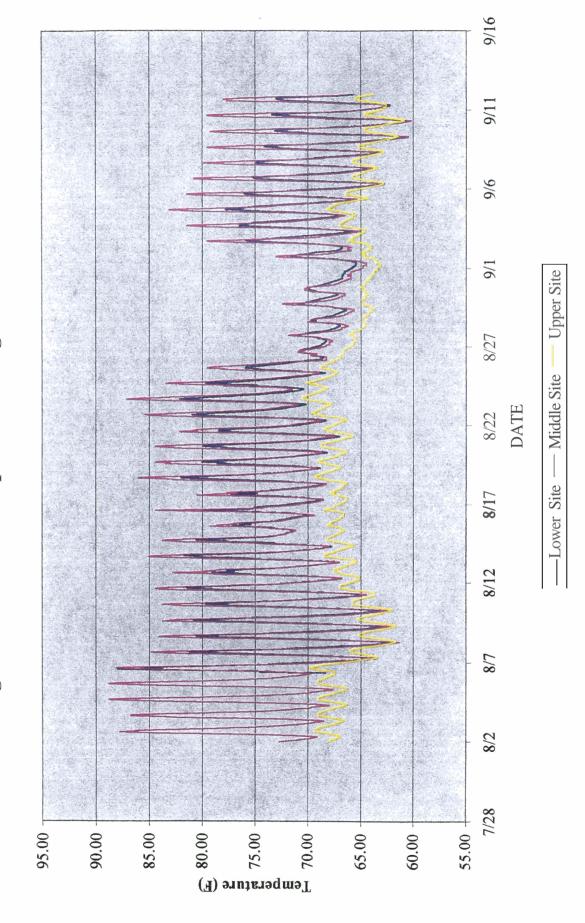




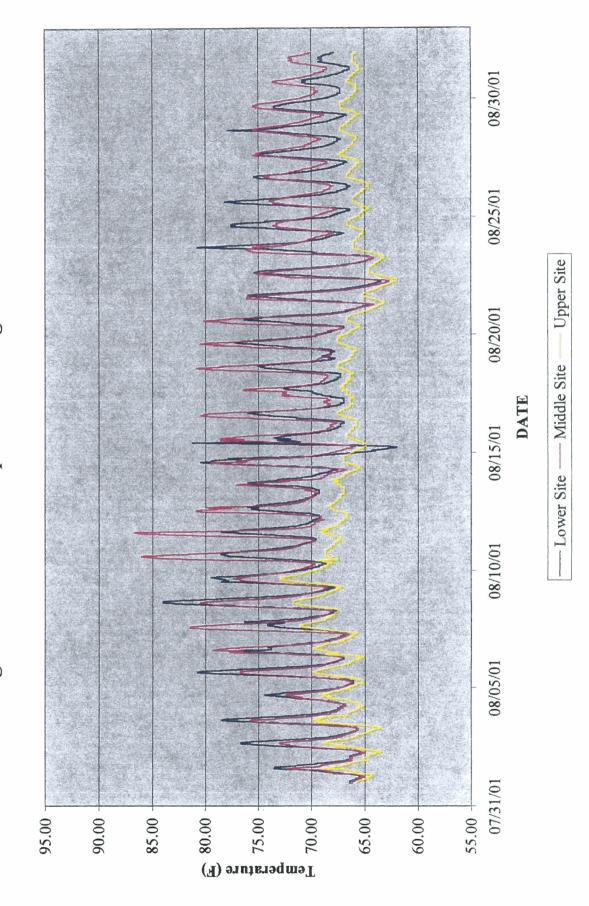


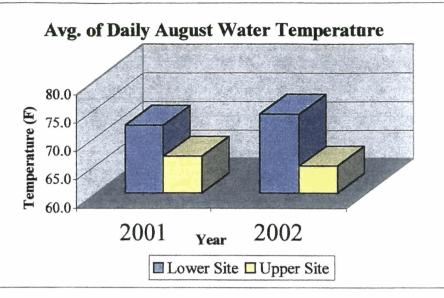


August 2002 Water Termperature on Big Warrior Creek

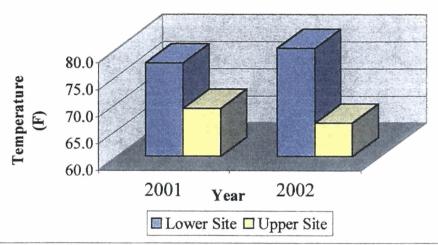


August 2001 Water Termperature on Big Warrior Creek

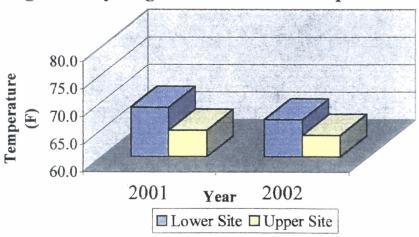




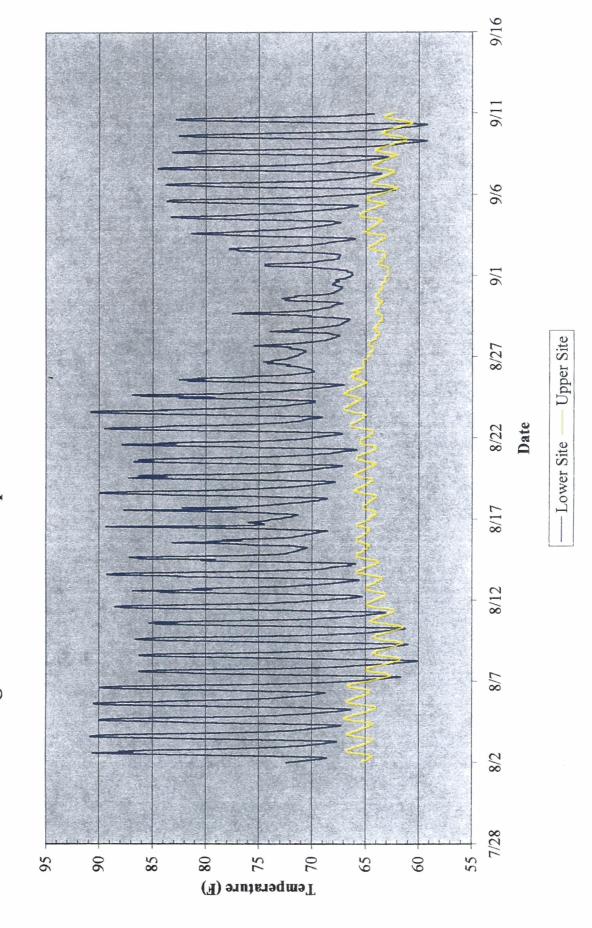




Avg. of Daily August Min. Water Temperature



August 2002 Water Temperature on Little Warrior Creek



August 2001 Water Temperature on Little Warrior Creek

